

# Reflection Seismic Method

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- Data and Image sort orders;
- Seismic Impedance;
- 2-D field acquisition geometries;
- CMP binning and fold;
- Resolution,
- Stacking charts;
- Normal Moveout and correction for it;
- Stacking;
- Zero-Offset reflection section;
- Migration.

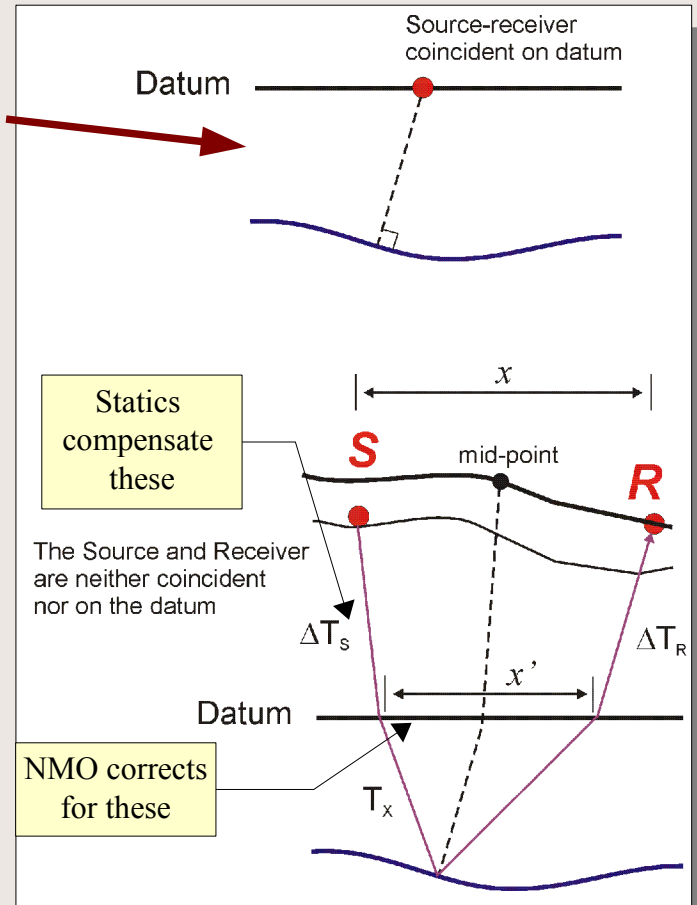
## • Reading:

- › Reynolds, Chapter 6
- › Shearer, 7.1-7.5
- › Telford *et al.*, Sections 4.3, 4.7, 4.8, 4.10

# Zero-Offset Section

*(The goal of reflection imaging)*

- **The ideal of reflection imaging** is sources and receivers *collocated* on a flat horizontal surface (“*datum*”).
- In reality, we have to record at *source-receiver offsets*, and over complex *topography*.
- **Two types of corrections** are applied to compensate these factors:



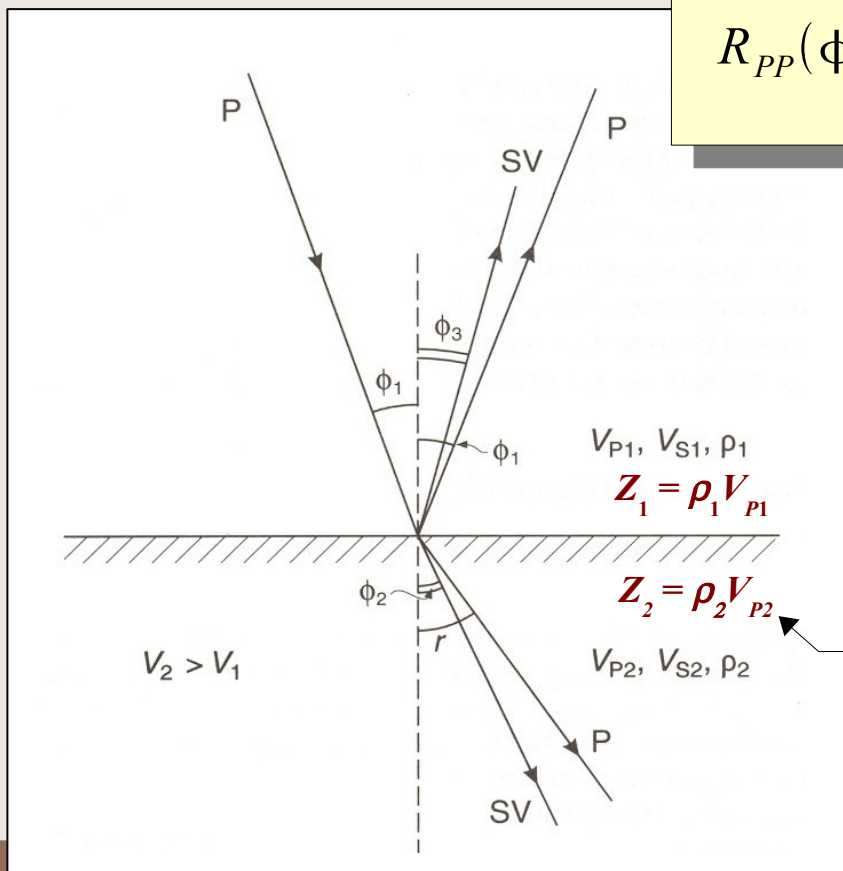
- **Statics** “place” sources and receivers onto the datum;
- Normal Moveout Corrections “transform” the records into as if they were recorded at collocated sources and receivers.
- **As a result** of these corrections (plus stacking to suppress noise), we obtain a *zero-offset section*.

# Reflection coefficient

*Quantity imaged in reflection sections*

- At *near-normal* incidence:
  - ♦ *P-to-S-wave conversions are negligible;*
  - ♦ *P-wave reflection and transmission amplitudes are determined by the contrast in **acoustic impedance**  $Z = \rho V$  (see next page).*
- *P- and S-wave reflection amplitudes usually **vary with incidence angles.***

$$R_{PP}(\phi) = \frac{A_{P_{reflected}}(\phi)}{A_{P_{incident}}(\phi)}$$



Acoustic impedance

# Acoustic Impedance

- Reflection-coefficient relations follow from: 1) continuity of displacement, and 2) conservation of energy upon reflection/transmission
- Acoustic impedance measures the energy flux within the wave:

$$E_{flux} = V E_{density} = V \frac{\rho}{2} (\omega A)^2 = \frac{\omega^2}{2} \rho V A^2$$

Kinetic energy

Z

## P-wave Reflection Coefficient

$$R_{PP} = \frac{A_{P_{reflected}}}{A_{P_{incident}}} = \frac{Z_2 - Z_1}{Z_2 + Z_1}$$

Note: if  $Z_2 < Z_1$ ,  $R < 0$ .  
This means *polarity reversal* upon reflection

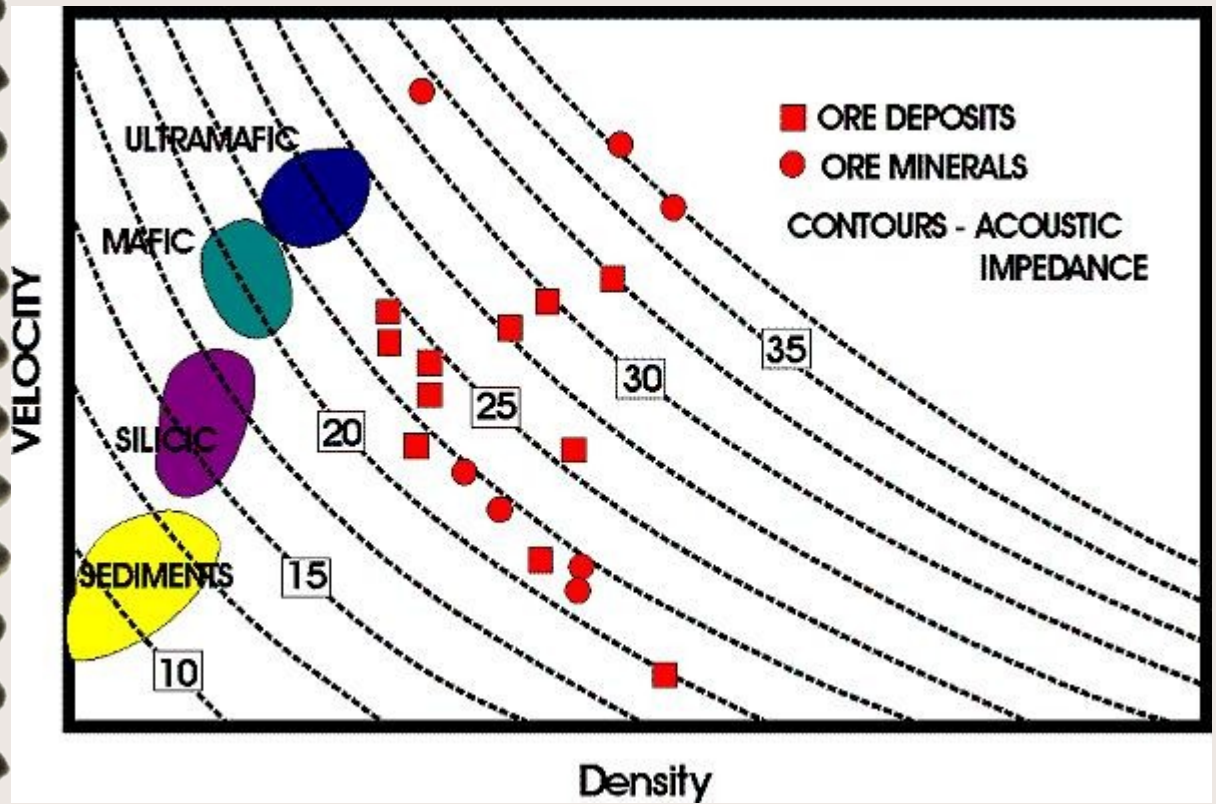
## P-wave Transmission Coefficient

$$T_{PP} = 1 - R_{PP} = \frac{2Z_1}{Z_1 + Z_2}$$

This follows from the continuity of displacement across the boundary

# Acoustic Impedance

## *Typical values*



*From Salisbury, 1996*

# Spatial resolution

- Two points are considered *unresolvable* when their reflection travel times are separated by less than *half the dominant period* of the signal:  $\delta t < T/2$ .

• Therefore,

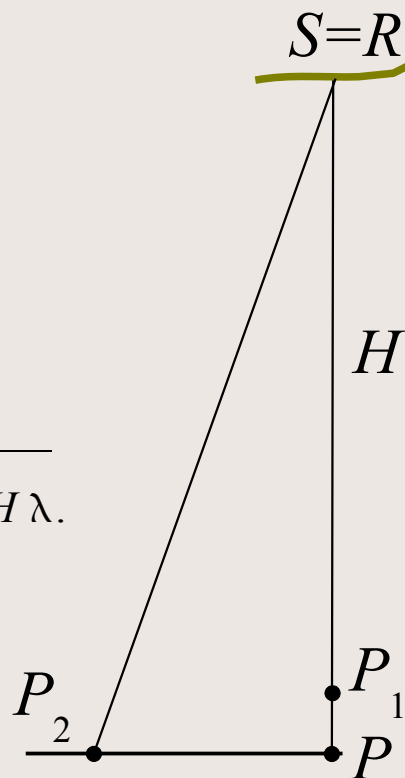
- vertical resolution:

$$\delta z = PP_1 = \frac{\lambda}{4}.$$

- horizontal resolution:

$$\delta x = PP_2 = \sqrt{\left(H + \frac{\lambda}{4}\right)^2 - H^2} \approx \sqrt{\frac{1}{2} H \lambda}.$$

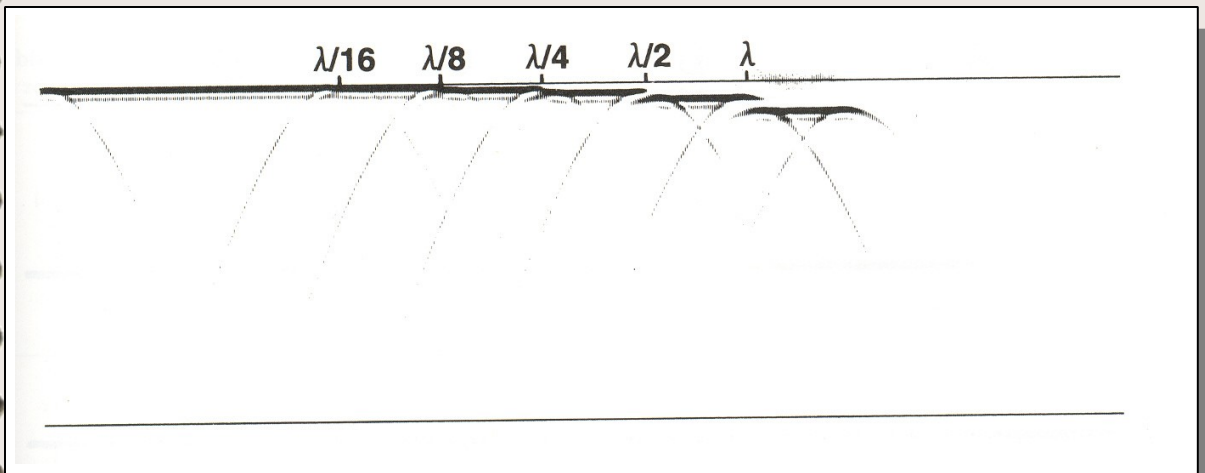
This is called  
*Fresnel Zone* radius



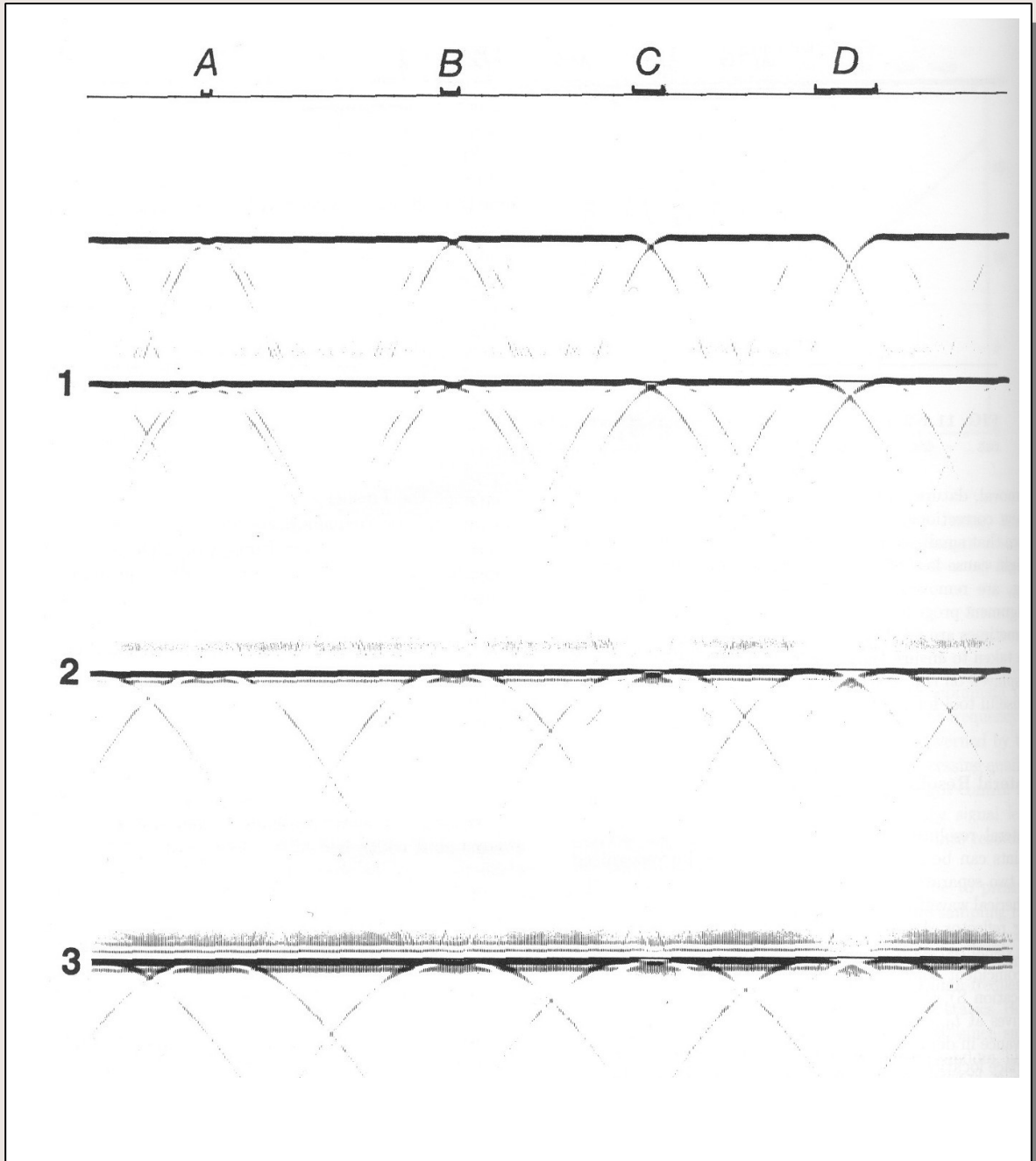
- Note that *horizontal resolution decreases with depth*.

# Vertical resolution

- Faults with different amounts of vertical throws, compared to the dominant wavelength:



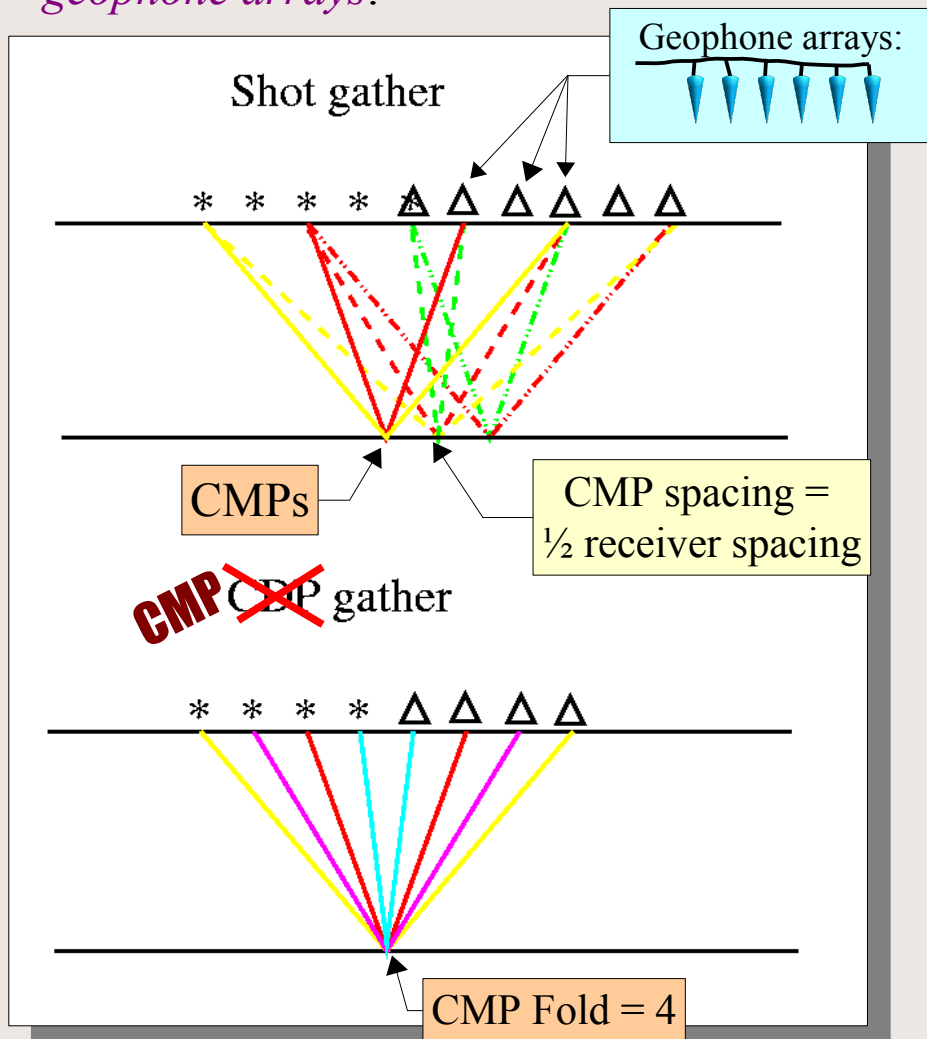
# Horizontal resolution





# Shot (field) and Common-Midpoint (image) sort orders

- Common-Midpoint survey:
  - ◆ Helps in reduction of random noise and multiples via *redundant coverage* of the subsurface;
  - ◆ Ground roll is attenuated through the use of *geophone arrays*.



# Field geometry

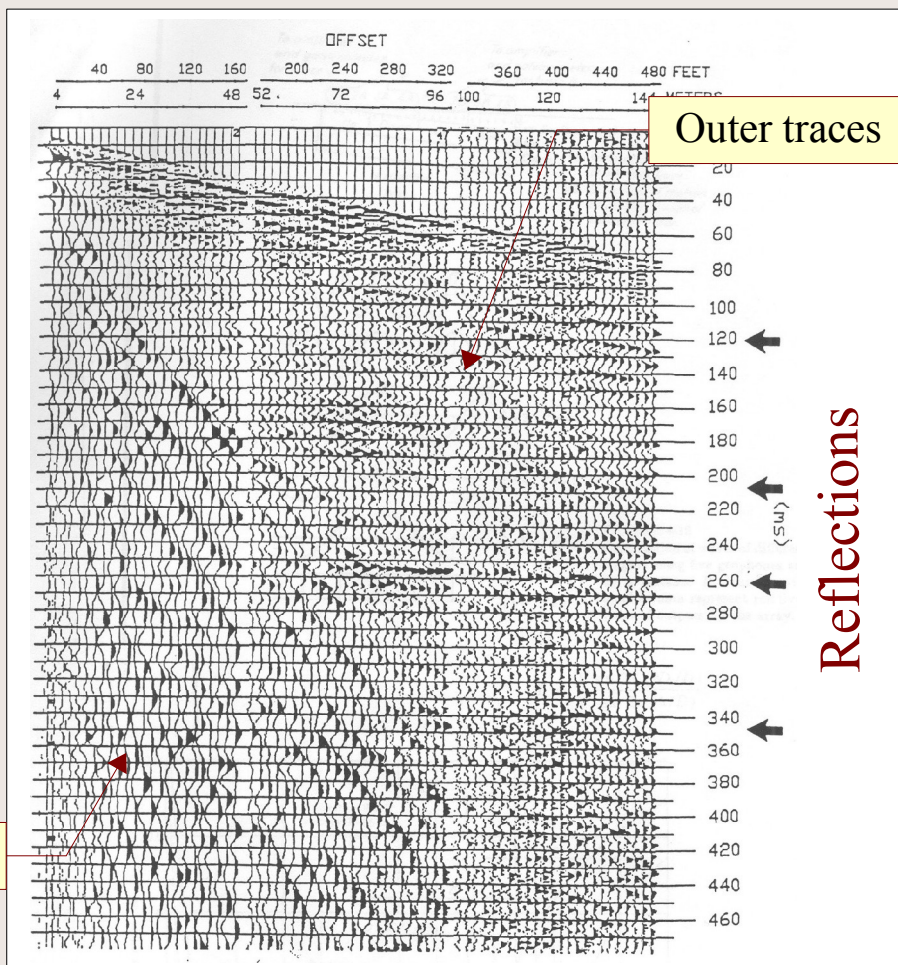
## survey and observer's logs, “chaining notes”

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- Survey file
  - ◆ Produced by surveyors (usually comes out of GPS unit);
- Observer's Notes
  - ◆ A record of shooting and recording sequence
    - Lists shot positions, record (“field file”) numbers (FFIDs), spread positions (“first live station”);
    - Records weather, interruptions, usual and unusual noise, state of recording system.

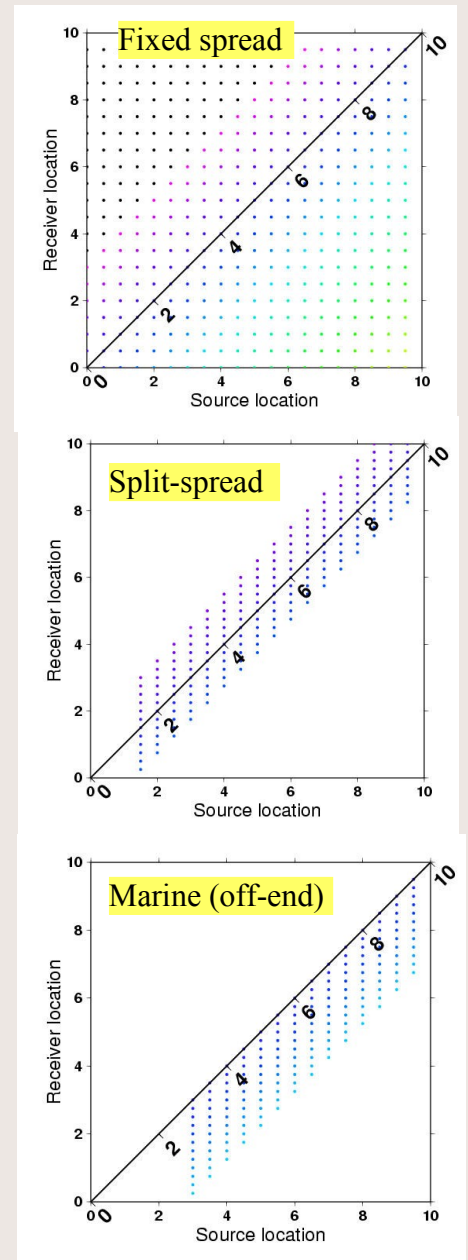
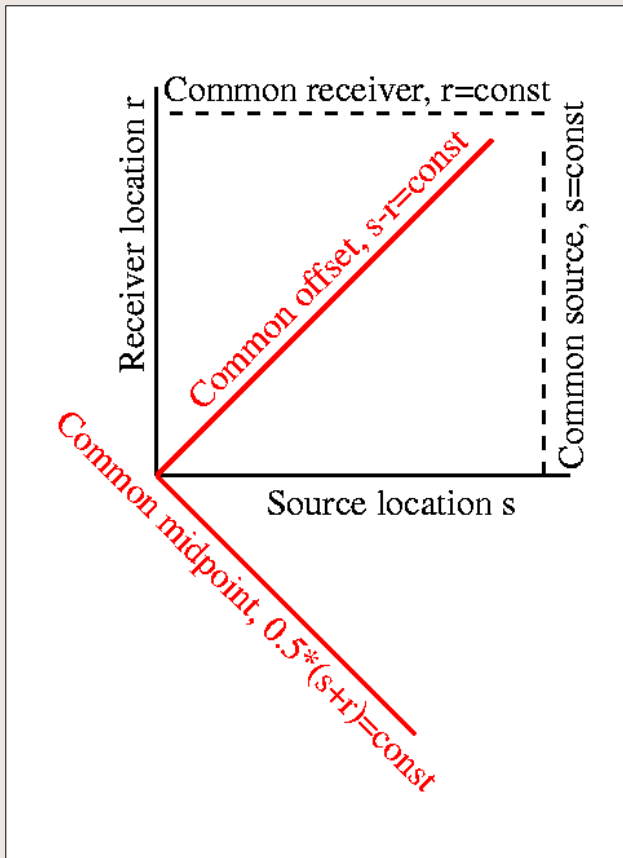
# Noise (Wave) Test

- Conducted prior to the acquisition in order to evaluate the appropriate survey design
  - ◆ Offset range;
  - ◆ Noise (ground roll, airwave) characteristics;
  - ◆ Offset range for useful reflections.



# Stacking chart

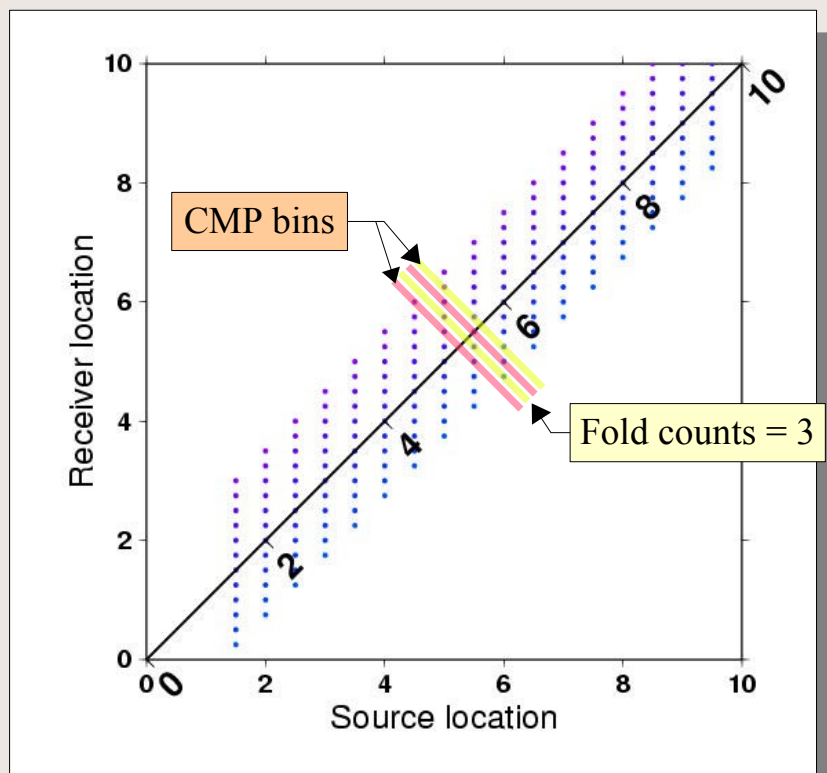
- Visualization of source-receiver geometry



# CMP Fold

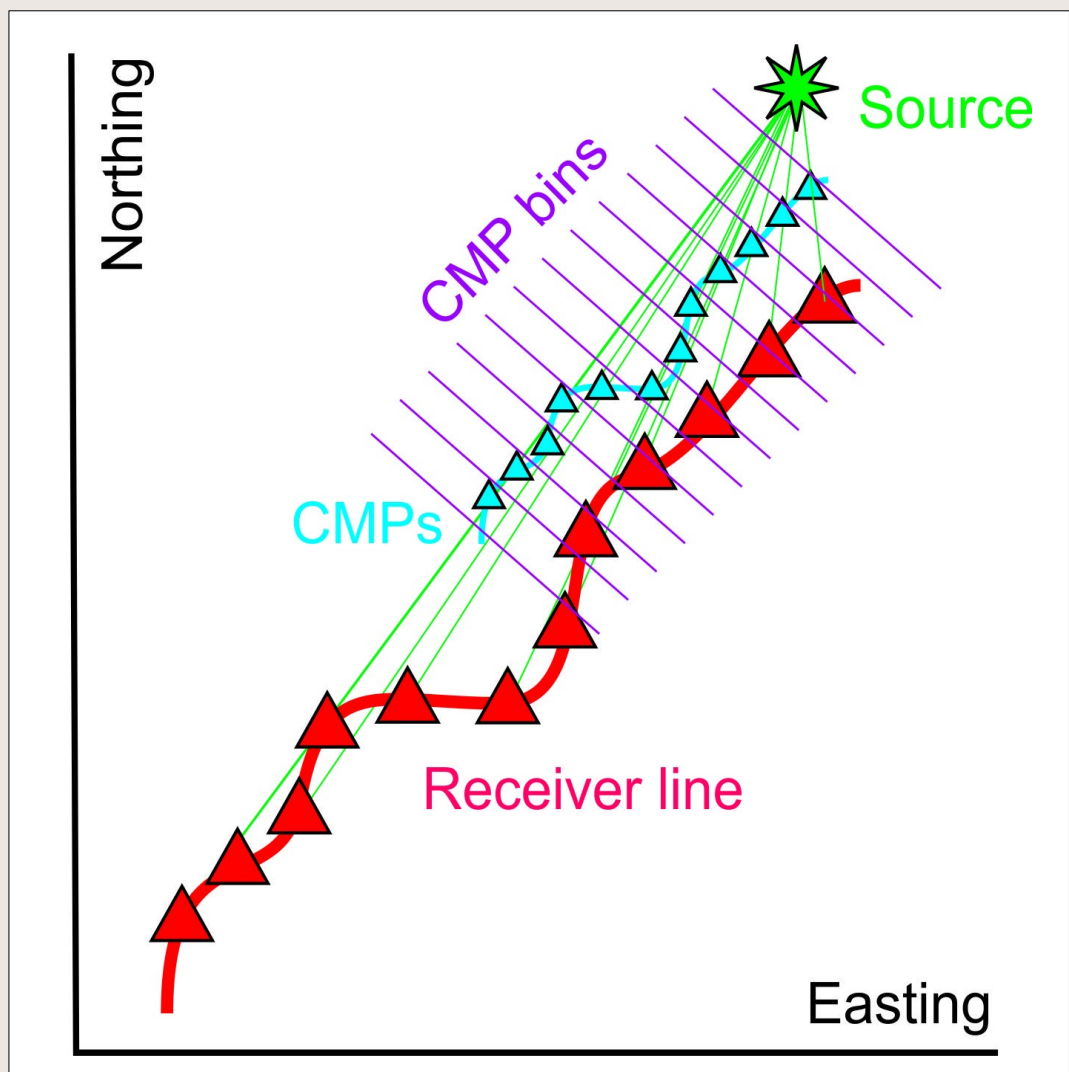
- Fold is the Number of records per CMP
  - ◆ Should be optimal (typically, 10-40);
  - ◆ Should be uniform (this is particularly an issue with 3D).

$$\text{Fold} = \frac{\text{Number of channels}}{2(\text{Num. of Shot point advances by Receiver spacing})}$$



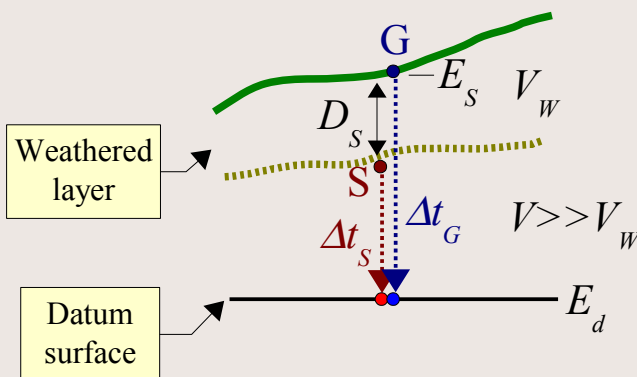
# Crooked-line binning

- Real seismic lines are often “crooked”
- CMP bins are then defined for an averaged, smooth line of midpoints



# Statics

- Statics are time shifts associated with source ( $\Delta t_S$ ) and receiver ( $\Delta t_R$ ) positions
  - ◆ When subtracted ('*applied*') from the travel-times, place the source and receiver on a common datum.
- (*Field statics*) = (*Elevation Correction*) + (*Weathering Correction*);
  - ◆ Elevation correction 'moves' the source and geophone to a common datum surface;
  - ◆ Weathering correction removes the effect of slow ( $\sim 600$  m/s) unconsolidated layer.
    - Obtained from *first arrivals*, using the plus-minus, GRM, or similar methods.
- Where field statics are not accurate enough, *residual statics* are also applied.

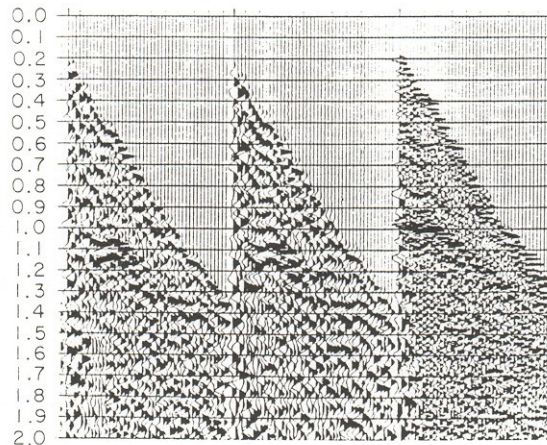


Elevation statics:

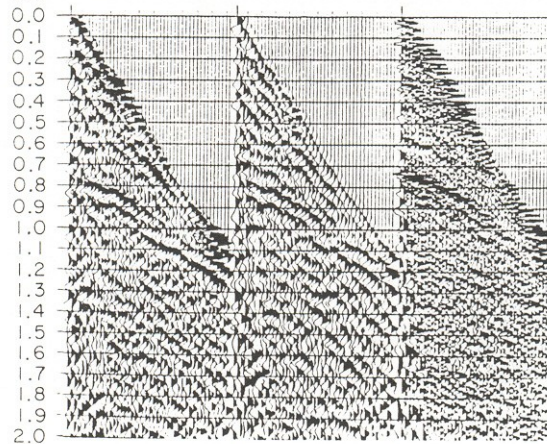
$$\Delta t_S = \frac{E_S - D_S - E_d}{V}$$

$$\Delta t_G = \Delta t_S + t_{uphole}$$

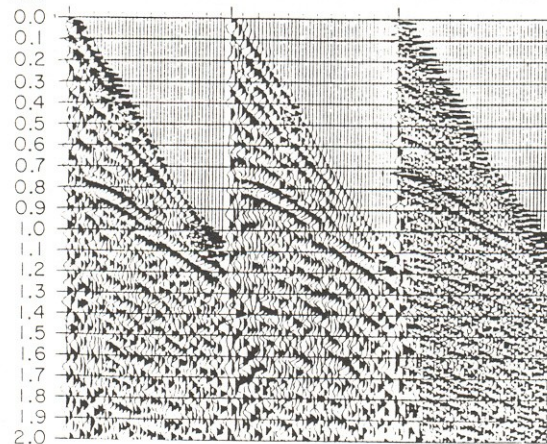
# Effects of statics in shot gathers



No statics



Conventional statics

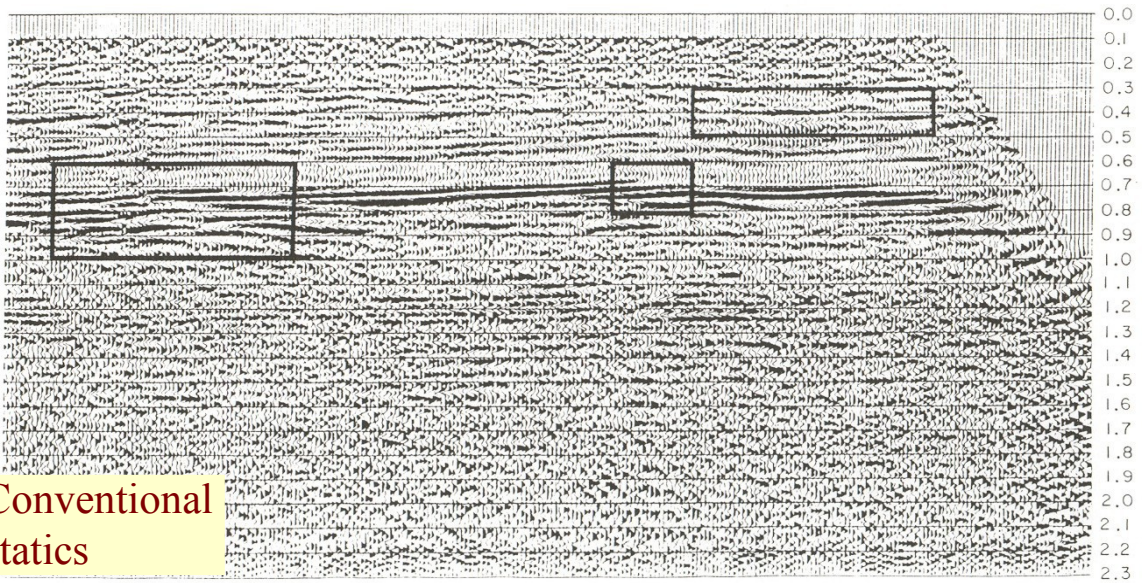


GLI  
(tomography)  
statics

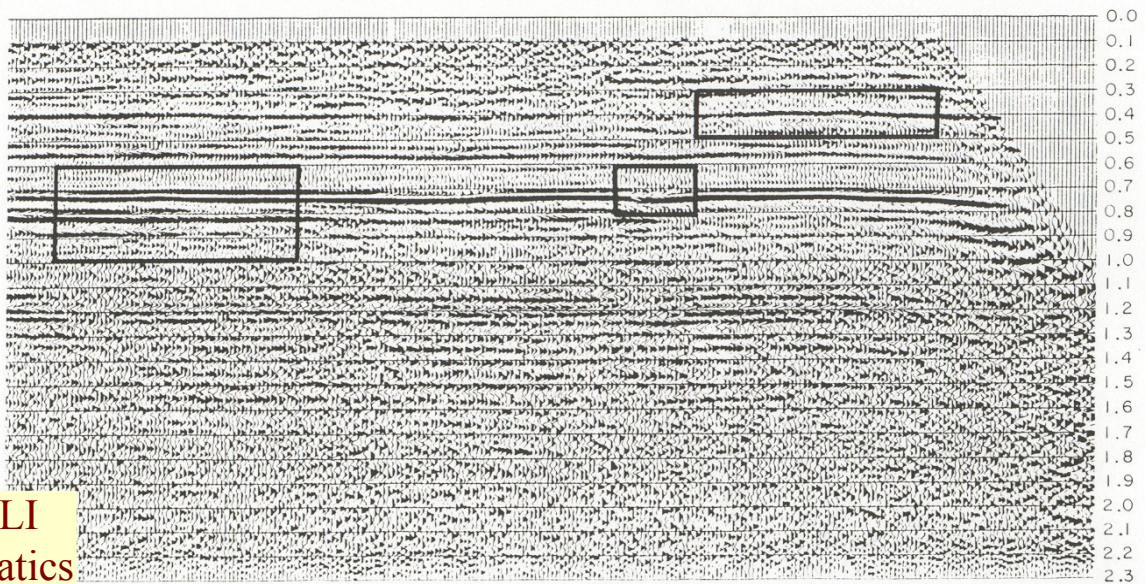


# Effects of statics in stacked image

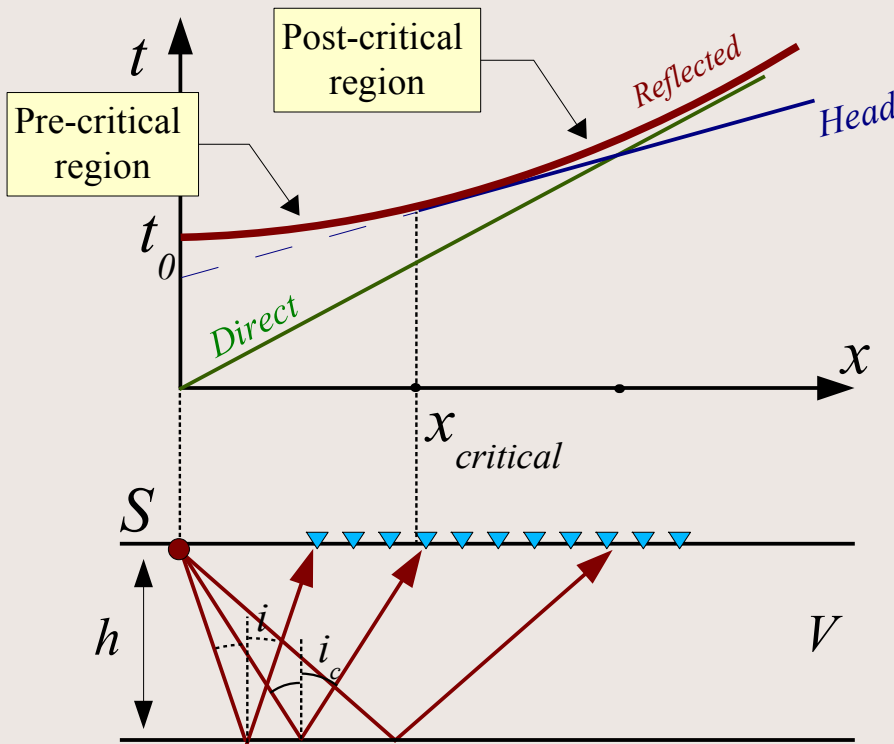
Conventional  
statics



GLI  
statics



# Reflection travel-times (Single layer)



$$t(x) = \frac{\sqrt{4h^2 + x^2}}{V} = \sqrt{\left(\frac{2h}{V}\right)^2 + \left(\frac{x}{V}\right)^2} = \sqrt{t_0^2 + \left(\frac{x}{V}\right)^2}$$

- $t(x)$  is called (hyperbolic) Normal reflection Moveout (NMO)

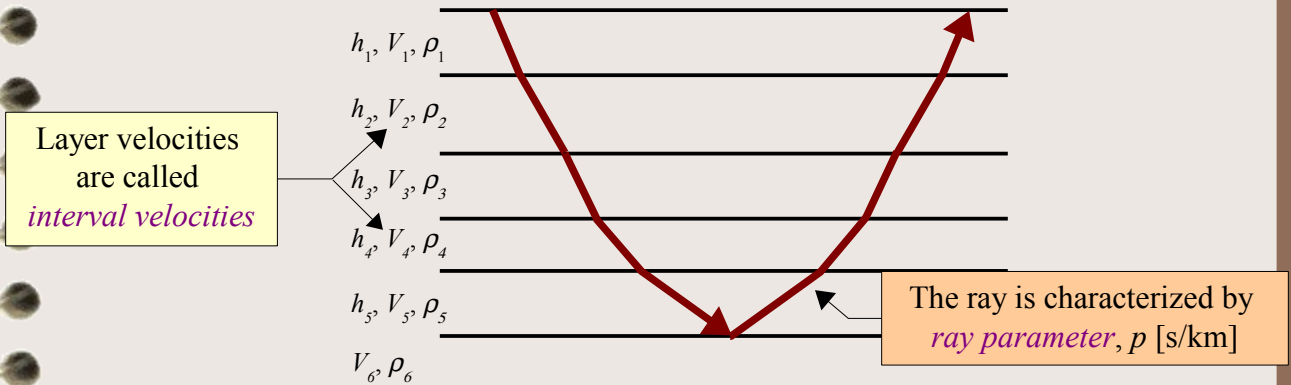
◆ Approximation for  $x \ll h$  (parabolic):

$$t(x) \approx t_0 + \frac{1}{2t_0} \left(\frac{x}{V}\right)^2$$

Note that deeper reflections in faster layers have smaller moveouts

# Reflection travel-times (Multiple layers)

- For multiple layers,  $t(x)$  is no longer hyperbolic:



- For practical applications (near-vertical incidence,  $pV_i \ll 1$ ),  $t(x)$  still can be approximated as:

$$x_n(p) = \sum_{i=1}^n \frac{h_i p V_i}{\sqrt{1 - (pV_i)^2}} \approx p \sum_{i=1}^n h_i V_i \left[ 1 + \frac{1}{2} (pV_i)^2 \right] \approx p \sum_{i=1}^n h_i V_i$$

hence: 
$$p = \frac{x_n(p)}{\sum_{i=1}^n h_i V_i}$$

$$t_n(p) = \sum_{i=1}^n \frac{h_i}{V_i \sqrt{1 - (pV_i)^2}} \approx \sum_{i=1}^n \frac{h_i}{V_i} \left[ 1 + \frac{1}{2} (pV_i)^2 \right] = t_0 + \frac{1}{2} p^2 \sum_{i=1}^n h_i V_i$$

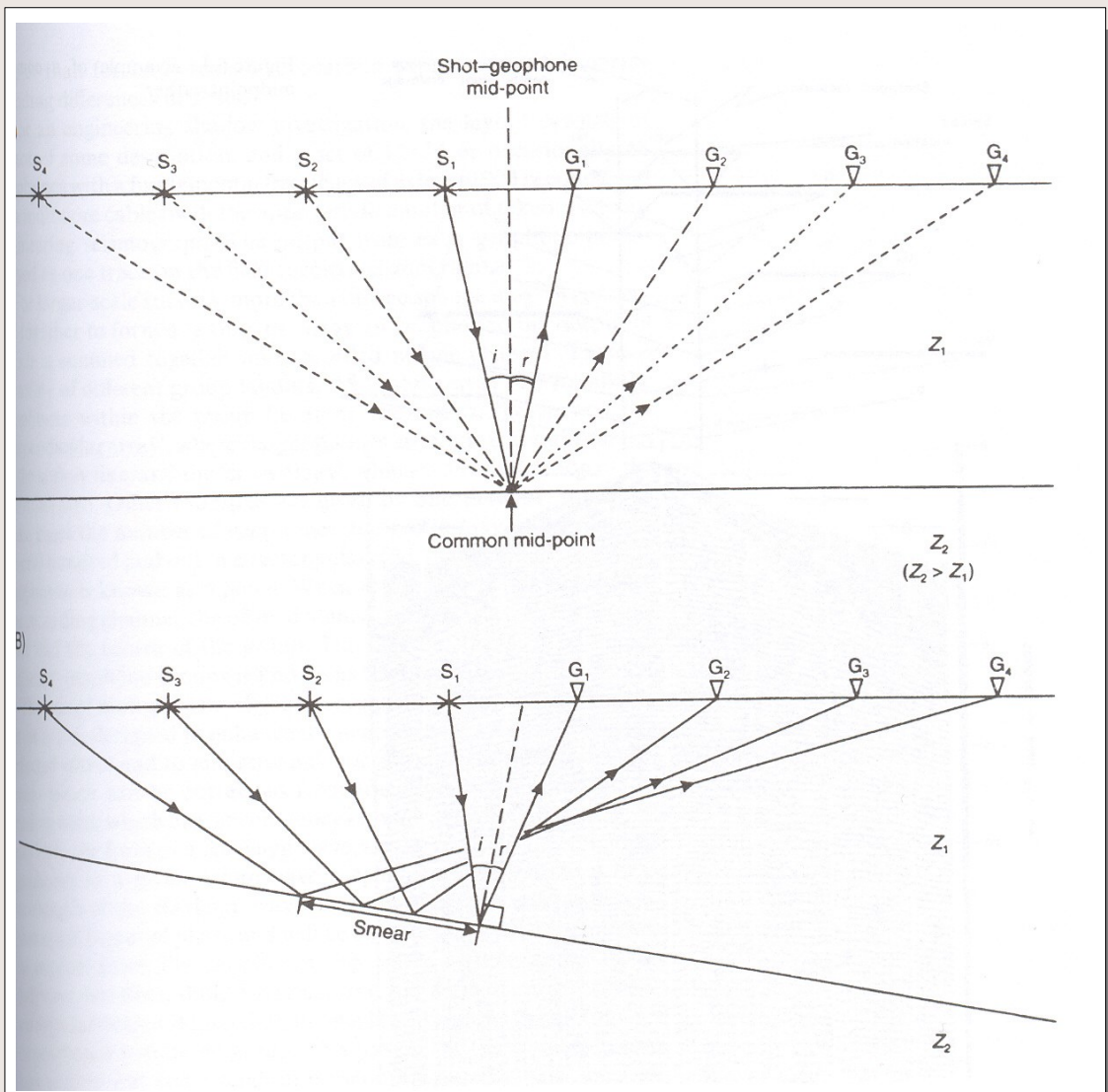
$$t_n(x) \approx t_0 + \frac{1}{2t_0} \left( \frac{x}{V_{RMS}} \right)^2$$

- where  $V_{RMS}$  is the RMS (root-mean-square) velocity:

$$V_{RMS} = \sqrt{\frac{\sum_{i=1}^n h_i V_i}{t_0}} = \sqrt{\frac{\sum_{i=1}^n t_i V_i^2}{\sum_{i=1}^n t_i}}$$

# Dipping reflector

- For a dipping reflector, the image is *smeared up-dip* and the stacking velocity is *over-estimated*.



# Measurement of velocities

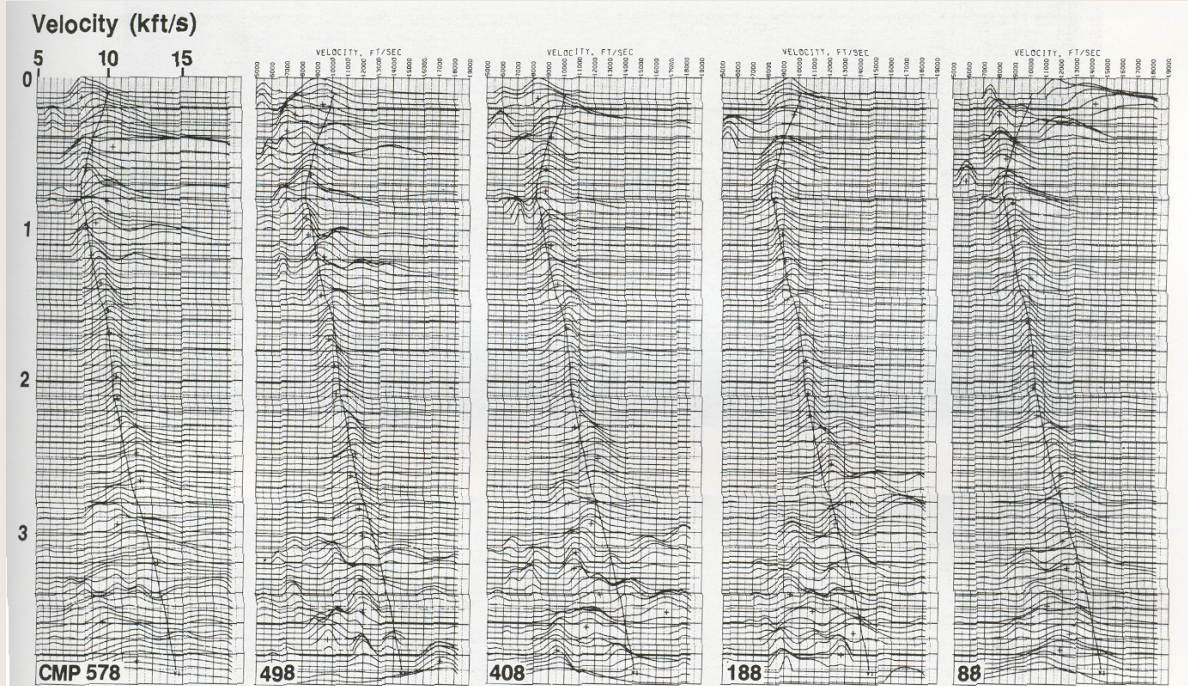
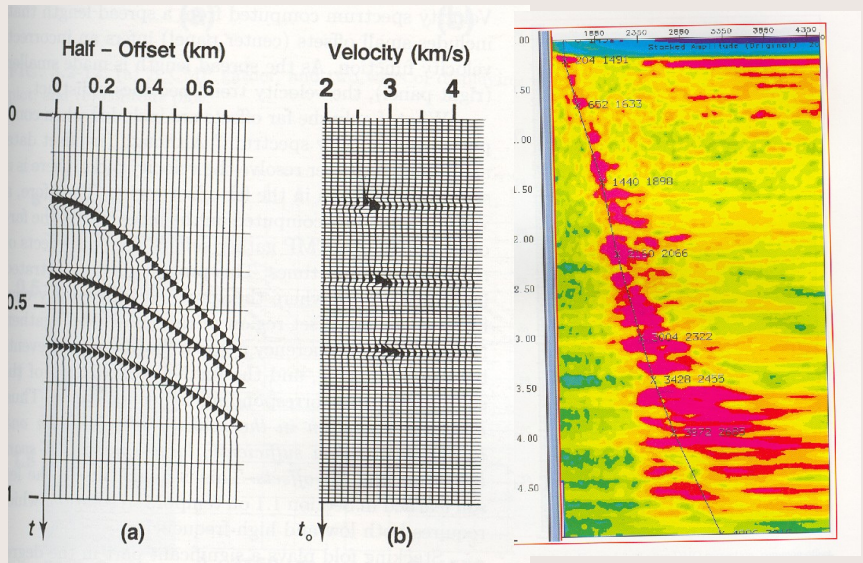
## (*Velocity analysis*)

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- Reflection (*stacking*) velocity analysis is usually performed in CMP gathers
  - ◆ because they pertain to specific locations within the subsurface.
- Travel-time approach -  $T^2$ - $X^2$  method:  $t^2(x^2)$  is a linear function. Slope of the graph in  $t^2(x^2)$  diagram is  $(1/V_{\text{Stacking}})^2$ .
- Waveform approach (*velocity spectrum* and *common velocity stacks (CVS)*)
  - ◆ stack the records along trial reflection hyperbolas;
  - ◆ plot the resulting amplitude in a  $(\text{time}, V_{\text{trial}})$  diagram;
  - ◆ pick amplitude peaks - this results in a  *$V(\text{time})$  profile*.

# Velocity Spectra

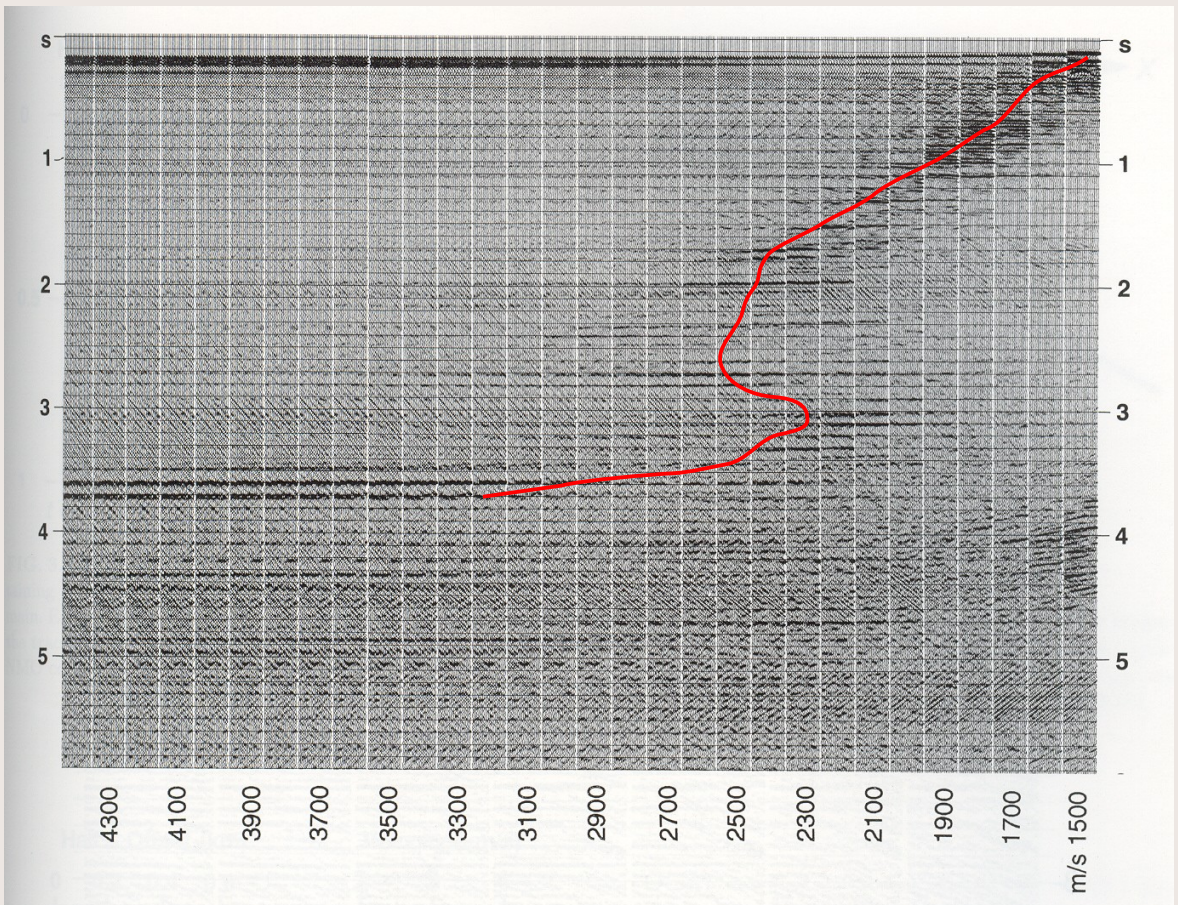
CMP gathers are stacked along trial velocities and presented in time-velocity diagrams.



# Common-Velocity Stacks

*(Velocity analysis)*

- CMP gathers are NMO-corrected (hyperbolas flattened) using a range of trial velocities and stacked.
- Velocities are picked at the amplitude peaks and best resolution in the stacks.



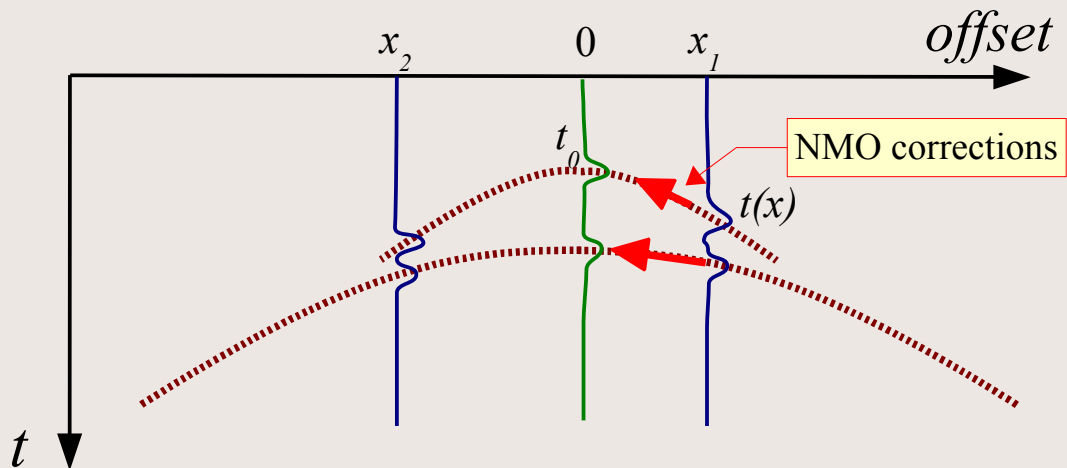
# Normal Moveout (NMO) correction

- NMO correction transforms a reflection record at offset  $x$  into a normal-incidence ( $x = 0$ ) record:

$$t(x) \rightarrow t_0 = t(x) - \delta t_{NMO}$$

$$\delta t_{NMO} = \sqrt{t^2 - \left(\frac{x}{V}\right)^2} - t_0 \approx \frac{1}{2t} \left(\frac{x}{V}\right)^2$$

“Stacking velocity”

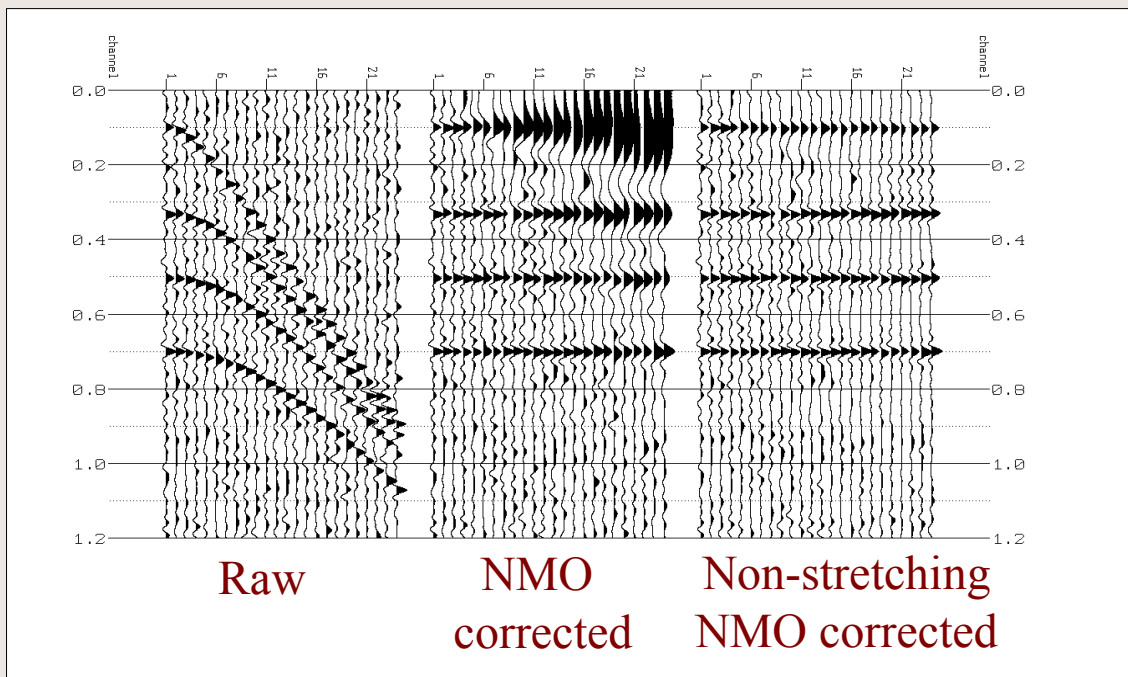


- Stacking velocity* is determined from the data, as a measure of the reflection hyperbola best aligned of with the reflection.



# NMO stretch

- NMO correction affects the shallower and slower reflections stronger
  - ◆ This is called “*NMO stretch*”
  - ◆ There is a considerable effort in creating “non-stretching” NMO algorithms

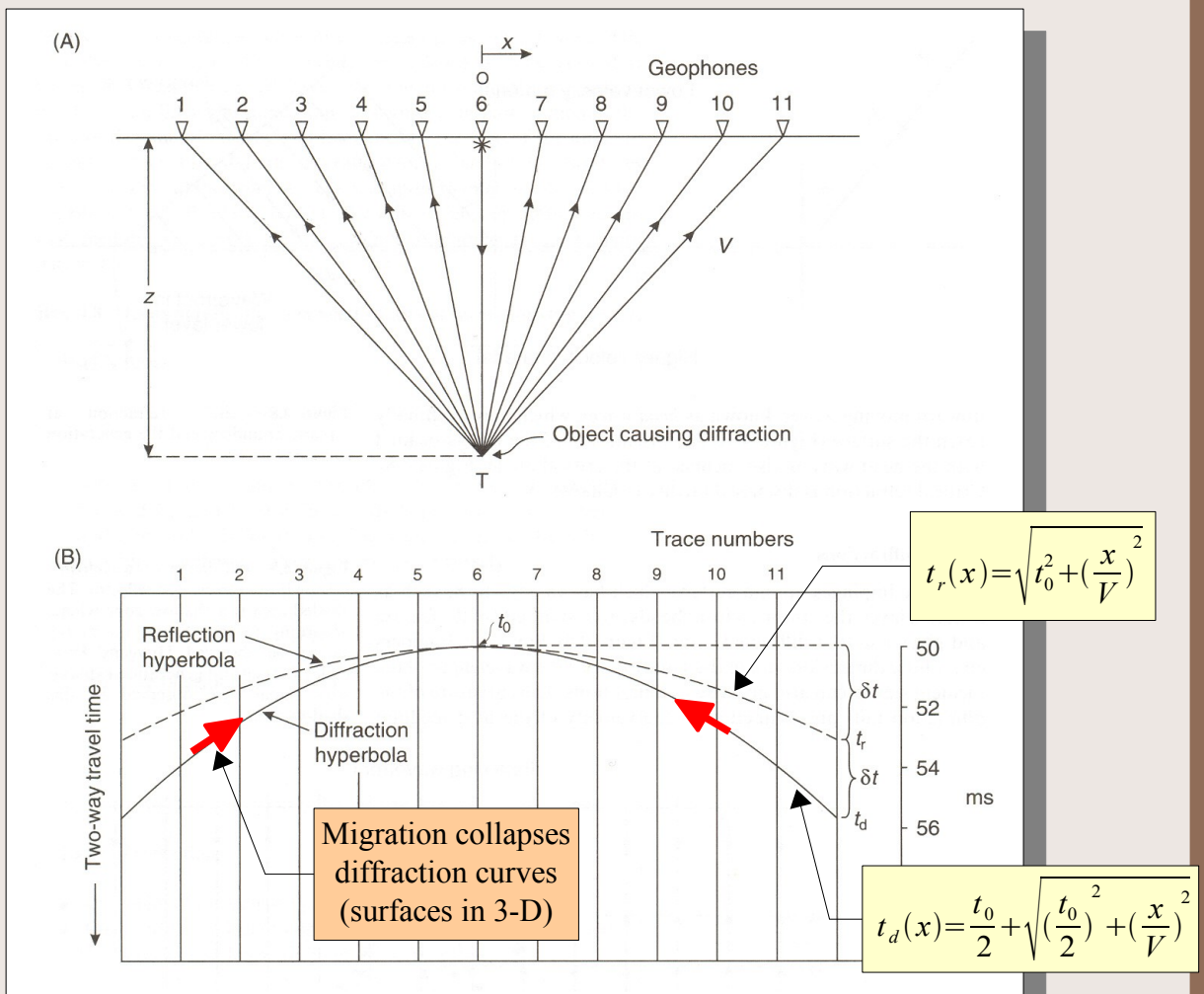


**Exercise:** derive the sensitivities of NMO correction to  $\delta t$ ,  $\delta V$ , and  $\delta x$ :

$$\partial(\delta t_{NMO})/\partial t, \partial(\delta t_{NMO})/\partial V, \partial(\delta t_{NMO})/\partial x.$$

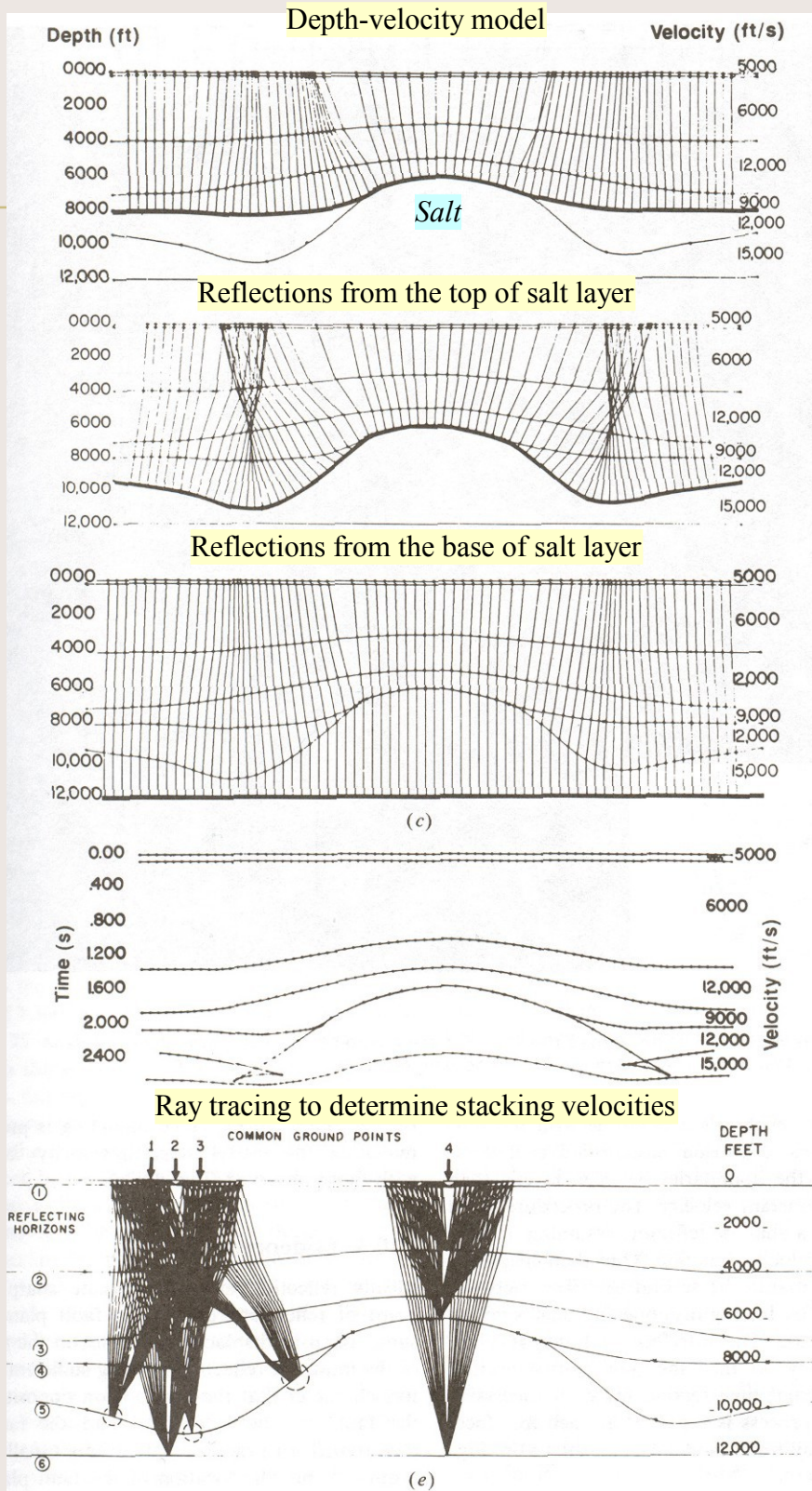
# Migration

- A simplified variant of '*inversion*'
  - ♦ Transforms the 'time section' into true '*depth image*'.
- Establishes true positions and dips of reflectors.
- Collapses diffractions.



# Modeling

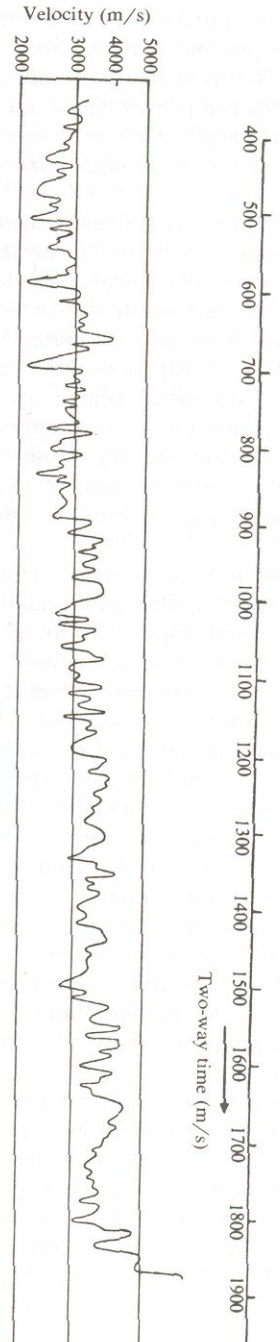
GEOL 335.3



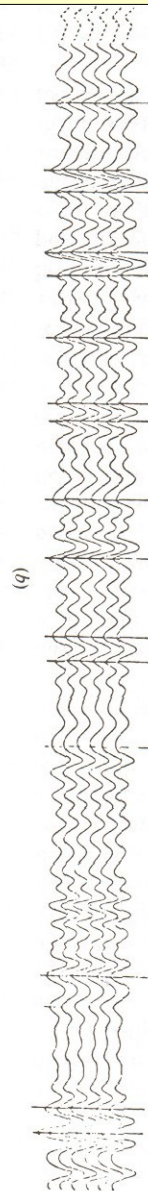
# Synthetic seismograms



Acoustic log



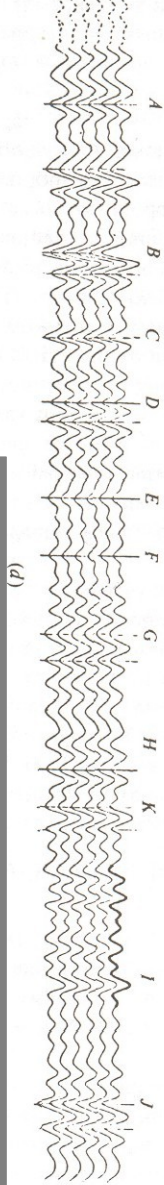
Synthetics  
(Convolved with  
wavelet)



Field data  
after NMO



Synthetics  
with  
principal  
multiples



Synthetics is spliced  
into CMP section  
for comparison

