Theory of Elasticity

- Macroscopic theory \bullet
- Equations of motion ٥
- Wave equations ٥
- Energy of a seismic wave Ø
	- **Reading:**
		- ➢ Telford et al., Section 4.2
	- ➢ Sheriff and Geldart, Sections 2.1-4

Stress

Consider the interior of a deformed Ø body: At point *P*, force *d***F** acts on

any infinitesimal area *dS. d***F** is a projection of *stress tensor*, σ, onto **n**:

 $dF_i = \sigma_{ij} n_j dS$

- Stress σ_{ij} is measured in [*Newton/m²*], or Pascal \bullet (unit of pressure).
- *d***F** can be decomposed into two components ٠ relative to the orientation of the surface, **n**:
	- Parallel (normal stress)

$$
(dF_n)_i = n_i \cdot
$$
 (projection of F onto n) $= (n_i \sigma_{kj} n_k n_j) dS$

Tangential (shear stress, *traction*)

 $d\vec{F}_\tau = d\vec{F} - d\vec{F}_n$ **b** $\frac{\text{column of }i}{\text{over }k \text{ and } j}$

Note summation

Forces acting on a small cube

- Consider a small parallelepiped (*dx* \bullet ×*dy*×*dz=dV*) within the elastic body.
- Exercise 1: show that the *force* applied \bullet to the parallelepiped from the outside is:

 $F_i = -\partial_j \sigma_{ij} dV$

(This is simply minus divergence (convergence?) of stress!)

Exercise 2: Show that *torque* applied to \bullet . the cube from the outside is:

Symmetry of stress tensor

- Thus, *L* is proportional to *dV: L = O*(*dV*) Ø
- The *moment of inertia* for any of the axes is ٥ proportional to *dV*·*length*²:

$$
I_x = \int_{dV} (y^2 + z^2) \rho dV
$$

and so it tends to 0 faster than *dV*: $I = o(dV)$.

Angular acceleration: $\theta = L/I$, must be *finite* as dV Ø, \rightarrow 0, and therefore:

$$
L_i/dV = -\epsilon_{ijk}\sigma_{jk} = 0.
$$

- Consequently, the stress tensor is *symmetric:* $\sigma_{ij} = \sigma_{ji}$ ٠
- \bullet

Strain

- **Strain is a measure of** deformation, i.e., *variation of relative displacement* as associated with a *particular direction* within the body
- It is, therefore, also a *tensor*
	- Represented by a matrix \bullet
	- Like stress, it is decomposed into \bullet *normal* and *shear* components
- Seismic waves yield strains of 10- $10 - 10^{-6}$
	- So we can rely on *infinitesimal* strain theory

Elementary Strain

- When a body is deformed, Ō *displacements* (**U**) of its points are dependent on (x,y,z), and consist of:
	- Translation (blue arrows below)

=

∂*Ui*

Deformation (red arrows)

Elementary strain is: \mathbb{C}

Stretching and Rotation

Exercise 1: Derive the elementary O strain associated with unidirectional stretching of the body along the *X* axis:

$$
\begin{pmatrix} x' \\ y' \end{pmatrix} = \begin{pmatrix} 1 + y & 0 \\ 0 & 1 + y \end{pmatrix} \begin{pmatrix} x \\ y \end{pmatrix}.
$$

Exercise 2: Derive the elementary \bullet strain associated with rotation by a small angle α :

$$
\begin{pmatrix} x' \\ y' \end{pmatrix} = \begin{pmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{pmatrix} \begin{pmatrix} x \\ y \end{pmatrix}.
$$

Strain Components

- Anti-symmetric combinations of e_{ij} yield Ō rotations of the body without changing its shape:
	- e.g., $\frac{1}{2}(\frac{\partial U_z}{\partial x}-\frac{\partial U_x}{\partial z})$ yields rotation about the 'y' axis. 2 $\left(\frac{\partial U_z}{\partial x} - \frac{\partial U_x}{\partial z}\right)$ \mathcal{E}
	- So, the case of $\frac{\sum z}{2} = \frac{\sum x}{2}$ is called *pure shear* (no rotation). ∂*U z* $rac{\partial U_z}{\partial x} = \frac{\partial U_x}{\partial z}$
- To characterize *deformation*, only the \mathbb{C}^n *symmetric* component of the elementary strain is used:

$$
\varepsilon_{ij} = \frac{1}{2} \left(\frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right),
$$

$$
\varepsilon_{ij} = \varepsilon_{ji}, \text{ where } i, j = x, y, \text{ or } z
$$

$$
\epsilon = \begin{pmatrix} \frac{\partial U_x}{\partial x} & \frac{1}{2} \left(\frac{\partial U_x}{\partial y} + \frac{\partial U_y}{\partial x} \right) & \frac{1}{2} \left(\frac{\partial U_x}{\partial z} + \frac{\partial U_z}{\partial x} \right) \\ \frac{1}{2} \left(\frac{\partial U_y}{\partial x} + \frac{\partial U_x}{\partial y} \right) & \frac{\partial U_y}{\partial y} & \frac{1}{2} \left(\frac{\partial U_y}{\partial z} + \frac{\partial U_z}{\partial y} \right) \\ \frac{1}{2} \left(\frac{\partial U_z}{\partial x} + \frac{\partial U_x}{\partial z} \right) & \frac{1}{2} \left(\frac{\partial U_z}{\partial y} + \frac{\partial U_y}{\partial z} \right) & \frac{\partial U_z}{\partial z} \end{pmatrix}
$$

Dilatational Strain (relative volume change during deformation)

- Original volume: *V*=δ*x*δ*y*δ*z* \bullet
- Deformed volume: *V+*δ*V=*(1+^ε *xx*) \bullet $(1+\varepsilon_{yy})(1+\varepsilon_{zz})\delta x \delta y \delta z$
- Dilatational strain: \bullet

$$
\Delta = \frac{\delta V}{V} = (1 + \varepsilon_{xx})(1 + \varepsilon_{yy})(1 + \varepsilon_{zz}) \approx \varepsilon_{xx} + \varepsilon_{yy} + \varepsilon_{zz}
$$

$$
\Delta = \varepsilon_{ii} = \partial_i U_i = \vec{\nabla} \vec{U} = \text{div } \vec{U}
$$

Note that *shearing strain does not* \bullet *change the volume*.

Hooke's Law (general)

- Hookes' law describes the stress Ō developed in a deformed body:
	- $F = -kx$ for an ordinary spring $(1-D)$
	- $\sigma \sim \varepsilon$ (in some sense) for a *'linear'*, *'elastic'* 3-D solid. This is what these terms mean:

For a general (*anisotropic*) medium, \bullet there are 36 coefficients of proportionality between six independent σ_{ii} and six ε_{ii} :

$$
\sigma_{ij} = \Lambda_{ij,kl} \epsilon_{kl}.
$$

Hooke's Law (isotropic medium)

For isotropic medium, the strain/stress O relation is described by just 2 constants:

$$
\sigma_{ij} = \lambda \Delta \delta_{ij} + 2 \mu \varepsilon_{ij}
$$

 $\delta_{_{ij}}$ is the "Kronecker symbol" (unit tensor) equal 1 for *i*=*j* and 0 otherwise;

λ and ^µ are called the *Lamé constants*.

- Although λ and μ provide a natural \bullet mathematical parametrization for $\sigma(\varepsilon)$, they are always intermixed in experimental environments.
	- Their combinations, called "*elastic modulae*" are typically directly measured.
- Question: what are the units for λ and μ ?

Four Elastic Modulae

- Depending on boundary conditions (i.e., Ø experimental setup), different combinations of λ' and μ may be convenient. These combinations are called *elastic constants*, or modulae:
	- Young's modulus and Poisson's ratio:
		- Consider a cylindrical sample uniformly squeezed along axis X:

Four Elastic Modulae

- Bulk modulus, K
	- Consider a cube subjected to hydrostatic pressure

- The constant μ complements K in describing the shear rigidity of the medium. Thus, μ is also called the '*rigidity modulus*'
- For rocks:
	- Generally, 10 Gpa $< \mu < K < E < 200$ Gpa
	- $0 < v < \frac{1}{2}$ always; for rocks, $0.05 < v < 0.45$, for most, ν is near 0.25.
- For liquids, $v=$ 1/2 and $\mu=0$ (no shear resistance)

Equations of Motion (Motion of the elastic body with time)

Uncompensated net force will result in Ø *acceleration* (Newton's law):

> ρ $\partial^2 U_{ij}$ $\frac{i}{2} = ($ ∂*ix* $\rho \delta V$ Newton's law:

∂*t*

$$
\rho \frac{\partial^2 U_x}{\partial t^2} = \frac{\partial}{\partial x} \left(\lambda' \Delta + 2\mu \frac{\partial U_x}{\partial x} \right) + \mu \frac{\partial}{\partial y} \left(\frac{\partial U_x}{\partial y} + \frac{\partial U_y}{\partial x} \right) + \mu \frac{\partial}{\partial z} \left(\frac{\partial U_x}{\partial z} + \frac{\partial U_z}{\partial x} \right)
$$

= $\lambda' \frac{\partial \Delta}{\partial x} + \mu \frac{\partial}{\partial x} \left(\frac{\partial U_x}{\partial x} + \frac{\partial U_y}{\partial y} + \frac{\partial U_z}{\partial z} \right) + \mu \left(\frac{\partial^2 U_x}{\partial x^2} + \frac{\partial^2 U_x}{\partial y^2} + \frac{\partial^2 U_x}{\partial z^2} \right)$
= $(\lambda' + \mu) \frac{\partial \Delta}{\partial x} + \mu \nabla^2 U_x$

• Therefore, the *equations of motion* for the components of **U**:

$$
\rho \frac{\partial^2 U_i}{\partial t^2} = (\lambda + \mu) \frac{\partial \Delta}{\partial x_i} + \mu \nabla^2 U_i
$$

∂ *x*

 $+\frac{\partial \sigma_{iy}}{2}$

∂ *y*

 $\partial^2 U_{i}$

∂*t*

 $+\frac{\partial \sigma_{iz}}{2}$

 $\frac{i}{2} = F_i$

∂ *z*

 $\overline{}$

Wave potentials

Compressional and Shear waves

- These equations describe two types of waves. 0
- The general solution has the form ("Lame ۰ theorem"):

$$
\vec{U} = \vec{\nabla} \phi + \vec{\nabla} \times \vec{\psi}.
$$
 (Of $U_i = \partial_i \phi + \epsilon_{ijk} \partial_j \psi_k$)

$$
\vec{\nabla} \cdot \vec{\psi} = 0.
$$
 Because there are 4 components
in ψ and ϕ only 3 in U, we need to constrain ψ .

Exercise: substitute the above into the Ø equation of motion:

$$
\rho \frac{\partial^2 U_i}{\partial t^2} = (\lambda + \mu) \frac{\partial \Delta}{\partial x_i} + \mu \nabla^2 U_i
$$

and show:

$$
\rho \frac{\partial^2 \phi}{\partial t^2} = (\lambda + 2\,\mu) \nabla^2 \phi, \quad \blacklozenge \quad \text{P-wave (scalar) potential.}
$$
\n
$$
\rho \frac{\partial^2 \psi_i}{\partial t^2} = \mu \nabla^2 \psi_i, \quad \blacktriangleleft \quad \text{S-wave (vector) potential.}
$$

Wave velocities

Compressional and Shear waves

These are wave equations; compare to the O general form of equation describing wave processes:

$$
\left[\frac{1}{c^2}\frac{\partial^2}{\partial t^2}-\nabla^2\right]f\left(x,y,z,t\right)=0
$$

Compressional (*P*) wave velocity:

$$
v_p = \sqrt{\frac{\lambda + 2\mu}{\rho}} = \sqrt{\frac{K + \frac{4}{3}\mu}{\rho}}
$$

Shear (*S*) wave velocity:

$$
\bullet \ \ V_{S} < \ V_{p}.
$$

for σ =0.25: V _{*P}*/ V _{*P*}= $\sqrt{3}$ </sub>

Note that the $V_{\beta}'V_{S}$ depends on the Poisson ratio alone:

$$
\frac{V_P}{V_S} = \sqrt{\frac{\mu}{\lambda + 2\,\mu}} = \sqrt{\frac{1/2 - \sigma}{1 - \sigma}}.
$$

 $v_{S} =$

Notes on the use of potentials

- Wave potentials are very useful for ٥ solving elastic wave problems
- Just take ϕ or ψ satisfying the wave equation, Ø e.g.:

$$
\phi(\vec{r},t) = Ae^{i\omega(t-\frac{\vec{r}\vec{n}}{V_p})}.
$$
 (plane wave)

...and use the equations for potentials to derive the displacements:

$$
\overrightarrow{\vec{U}} = \vec{\nabla} \phi + \vec{\nabla} \times \vec{\psi}.
$$

...and stress from Hooke's law:

$$
\sigma_{ij} = \lambda \Delta \delta_{ij} + 2\mu \varepsilon_{ij}
$$

Displacement amplitude = Ø

$$
a \times (potential\ amplitude)/V
$$

Power = $\frac{1}{2}$ *p*[ω^2 *×*(*potential amplitude*)/*V*]²

This is *velocity* amplitude

Example: Compressional (*P*) wave

- Scalar potential for *plane harmonic* wave: Ø $i \omega (t - \frac{\vec{r} \cdot \vec{n}}{2})$ $\overline{}$ $\phi(\vec{r},t)=Ae$ *V ^P* .
	- Displacement: $u_i(\vec{r},t) = \partial_i \phi(\vec{r},t) = \frac{-i \omega n_i}{V}$ *V P Ae* $i \omega (t - \frac{\vec{r} \cdot \vec{n}}{2})$ *V ^P* $\overline{}$.

note that the displacement is always along **n**.

Ø Strain:

Ø

$$
\varepsilon_{ij}(\vec{r},t) = \partial_i u_j(\vec{r},t) = \frac{\omega^2 n_i n_j}{V_P^2} A e^{i\omega(t - \frac{\vec{r}\vec{n}}{V_P})}.
$$

Dilatational strain: Ø

$$
\Delta = \varepsilon_{ii}(\vec{r},t) = \frac{\omega^2}{V_P^2} A e^{i\omega(t-\frac{\vec{r}\vec{n}}{V_P})} = \frac{\omega^2}{V_P^2} \phi(\vec{r},t).
$$

Stress: extended a stress of the stress

$$
\sigma_{ij}(\vec{r},t) = \frac{\omega^2}{V_p^2} (\lambda \delta_{ij} + 2 \mu n_i n_j) \phi(\vec{r},t).
$$

Question: what wavefield would we have if used cos() or sin() function instead of complex exp() in the expression for potential above?

Impedance

- *Impedance, Z,* is a measure of the O amount of resistance to particle motion.
- In elasticity, impedance is a *ratio of* ۵ *stress to particle velocity*.
	- Thus, for a given applied stress, ۰ particle velocity is inversely proportional to impedance.
	- ◆ For *P* wave, in the direction of its propagation:

$$
Z(\vec{r},t) = \frac{\sigma_{nn}(\vec{r},t)}{\mu_n(\vec{r},t)} = \frac{\lambda + 2\mu}{V_P} = \rho V_{P}.
$$

➔ impedance does not depend on frequency but *depends on the wave type and incidence direction.*

Elastic Energy Density

- Mechanical work is required to deform Q an elastic body; as a result, elastic energy is accumulated in the strain/stress field
- When released, this energy gives rise to \bullet earthquakes and seismic waves
- For a loaded spring (1-D elastic body), ۰ *E*= ½*kx*2=½*Fx*
- Similarly, for a deformed elastic Ø medium, *energy density* is:

$$
E = \frac{1}{2} \sigma_{ij} \epsilon_{ij}
$$

Elastic Energy Density *in a plane wave*

For a plane wave: \bullet

$$
u_{i} = u_{i} (t - \vec{p} \cdot \vec{x})
$$

$$
\varepsilon_{ij} = \frac{1}{2} (\partial_{i} u_{j} + \partial_{j} u_{i}) = -\frac{1}{2} (\dot{u}_{i} p_{j} + \dot{u}_{j} p_{i}).
$$

a ...and therefore:

$$
\frac{1}{2}\sigma_{ij}\varepsilon_{ij} = \frac{1}{2}[(\lambda + \mu)(\vec{p}\cdot\vec{u})^2 + \mu(\vec{u}\cdot\vec{u})(\vec{p}\cdot\vec{p})]
$$

For *P*- and *S*-waves, this gives: Ø

$$
\frac{1}{2}\sigma_{ij}\varepsilon_{ij} = \frac{1}{2}(\lambda + 2\mu) p^2 \vec{u}^2 = \frac{1}{2}\rho \dot{\vec{u}}^2
$$
 P-wave

$$
\frac{1}{2}\sigma_{ij}\varepsilon_{ij} = \frac{1}{2}(\mu) p^2 \vec{u}^2 = \frac{1}{2}\rho \dot{\vec{u}}^2
$$
 S-wave

- Thus, in a wave, *strain energy equals* O *the kinetic energy* Energy is *NOT* conserved locally!
- *Energy propagates at the same speed* \bullet as the wave pulse

Wave Polarization

 Elastic solid supports two types of Ø *body waves*:

