

Lecture 5: Lagrangian Mechanics of Continuous Media

- Key concepts of classical mechanics of continuous solids
 - Strain, stress
 - Elasticity, viscosity
 - Lagrangian and dissipation functions
 - Hooke's law, Navier-Stokes law
 - Media with internal structure ("General Linear Solid", GLS)
 - Two types of GLS models
 - Equations of motion
 - Extensions of the model: nonlinearity, thermal effects, anisotropy
 - Effective media
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- Reading: Sections 5.1 – 5.3 in the text

Lagrangian approach

- Here, we will consider weak reversible deformations of isotropic solid or liquid materials
 - Solid and liquids obey generally the same laws in small deformations
- Like with any problem in physics, to determine the motion of a solid body, we need to:
 1. Identify the generalized coordinates (parameters of deformation)
 2. Specify the Lagrangian (L) and dissipation function (D)
 3. From functions L and D , Determine the generalized forces, momenta, energies and establish the conservation laws
 4. The relations of forces to parameters of deformation (displacements, strains) will give the constitutive relations
 5. Write the Euler-Lagrange equations. They will be the equations of motion.
 6. Solve the equations of motion with appropriate boundary conditions representing the shape of the body, thermal regime, external forces, etc.
- Note that the construction of Lagrangian and dissipation functions is based on general principles of linearity, scales, and symmetries
 - Therefore, all possible interactions are included in the obtained equations

Description of deformation

- To describe deformation of a continuous body, we use several fields (plot on the right):

- Displacement vector $\mathbf{u}(\mathbf{x})$ of each point \mathbf{x} (blue and red in the figure). Its components are the generalized variables for deformation.
- To obtain the Lagrangian and dissipation function, additional quantities are derived from $\mathbf{u}(\mathbf{x})$:

- “Elementary strain” tensor: $e_{ij} = \frac{\partial u_i}{\partial x_j} \equiv \partial_i u_j$, where $i, j = [x, y, z]$ or $[1, 2, 3]$

- Strain tensor: $\varepsilon_{ij} = \frac{1}{2}(e_{ij} + e_{ji}) = \frac{1}{2}\left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i}\right)$ This symmetric tensor excludes rotations from e_{ij}

- Dilatational (volumetric) strain Δ (scalar quantity, relative volume change).

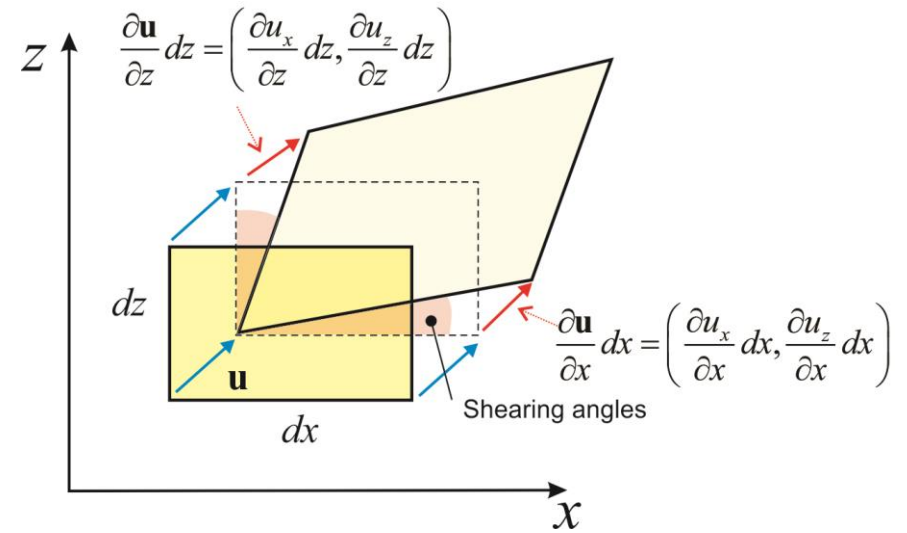
Several expressions for it:

$$\Delta = \frac{\delta V}{V} = (1 + \varepsilon_{xx})(1 + \varepsilon_{yy})(1 + \varepsilon_{zz}) - 1 \approx \varepsilon_{xx} + \varepsilon_{yy} + \varepsilon_{zz}$$

$$\Delta = \frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = \partial_i u_i$$

$$\Delta = \text{div} \mathbf{u} = \nabla \cdot \mathbf{u}$$

- Deviatoric (shear) strain: $\tilde{\varepsilon}_{ij} = \varepsilon_{ij} - \frac{\Delta}{3} \delta_{ij}$ This tensor contains no volume change: $\text{tr} \tilde{\varepsilon} = \tilde{\varepsilon}_{ii} = 0$

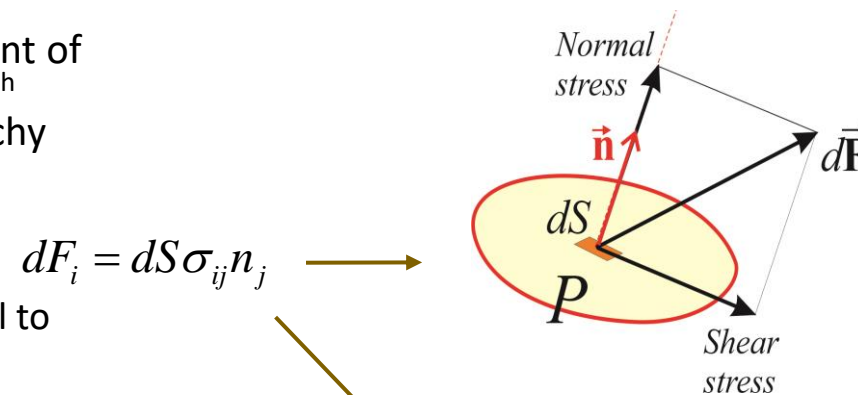
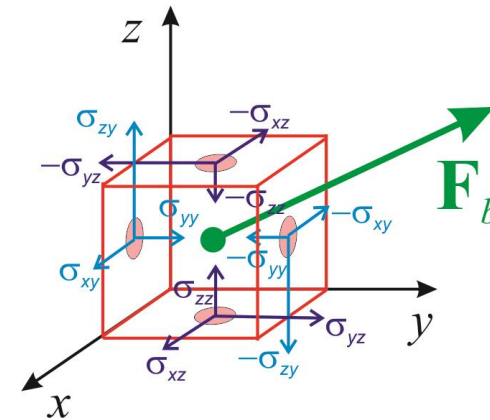


This tensor excludes translations from u_i and describes the change of shape of yellow rectangle above

$$\boldsymbol{\varepsilon} = \begin{pmatrix} \frac{\partial u_x}{\partial x} & \frac{1}{2} \left(\frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right) & \frac{1}{2} \left(\frac{\partial u_x}{\partial z} + \frac{\partial u_z}{\partial x} \right) \\ \frac{1}{2} \left(\frac{\partial u_y}{\partial x} + \frac{\partial u_x}{\partial y} \right) & \frac{\partial u_y}{\partial y} & \frac{1}{2} \left(\frac{\partial u_y}{\partial z} + \frac{\partial u_z}{\partial y} \right) \\ \frac{1}{2} \left(\frac{\partial u_z}{\partial x} + \frac{\partial u_x}{\partial z} \right) & \frac{1}{2} \left(\frac{\partial u_z}{\partial y} + \frac{\partial u_y}{\partial z} \right) & \frac{\partial u_z}{\partial z} \end{pmatrix}$$

Description of forces

- Two types of forces can act on an elementary volume within rock (REV; **plot on the upper-right**):
 - Body force** \mathbf{F}_b applied to the whole volume and proportional to its volume dV (**green**)
 - Surface forces** applied to the six faces of the REV, proportional to their surface areas dS . The i^{th} component of force per unit area applied to the face oriented in the j^{th} direction is denoted σ_{ij} . These components form a Cauchy stress tensor σ (matrix; **bottom right**)
 - Definition of surface force through the stress tensor (**middle plot and matrix product in the bottom**):
 - It can be decomposed to normal component (parallel to normal vector \mathbf{n}) and tangential (shear, traction)
 - The **stress tensor is always symmetric** because of the invariance of the elastic energy with respect to rotation of the frame of reference
- Both of these types of forces can in principle exist for both elasticity and friction (viscosity)
 - However, body forces do not exist for ordinary material without internal structure



$$\begin{pmatrix} dF_x \\ dF_y \\ dF_z \end{pmatrix} = dS \begin{pmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{pmatrix} \begin{pmatrix} n_x \\ n_y \\ n_z \end{pmatrix},$$

$\sigma_{xy} = \sigma_{yx}$,
 $\sigma_{xz} = \sigma_{zx}$,
 $\sigma_{yz} = \sigma_{zy}$

Shear stress components are symmetric (pointing to the off-diagonal elements in the matrix)
Normal stress components (pointing to the diagonal elements in the matrix)

Forming the Lagrangian and dissipation function

- Here are **the general rules** for defining the Lagrangian (almost the same rules apply to the dissipation function):

1. The Lagrangian of the body is a functional of the displacement field $\mathbf{u}(\mathbf{x}, t)$ and its time derivative (velocity field) $\dot{\mathbf{u}}(\mathbf{x}, t)$

This means that current displacement and velocities uniquely determine all future motion of the rock

2. The Lagrangian of the whole body is an integral of the **Lagrangian density function** L : $L\{\mathbf{u}, \dot{\mathbf{u}}\} = \int L dV$

This means that the interactions are local within volume dV

3. At point \mathbf{x} , the density function L depends on the displacement vector \mathbf{u} , velocity $\dot{\mathbf{u}}$, and strain tensor $\boldsymbol{\varepsilon}$

But it does not depend on stress $\boldsymbol{\sigma}$ or derivatives of $\boldsymbol{\varepsilon}$, for example!

4. To describe **linear interactions**, L must be a **quadratic function** of $\mathbf{u}(\mathbf{x}, t)$ and its derivatives

5. To describe a linear **isotropic medium**, L should be a function of quadratic scalar invariants derived from \mathbf{u} and $\boldsymbol{\varepsilon}$. Such invariants are:

- Square of displacement (or velocity) vector $|\mathbf{u}|^2 = u_i u_i$
- Two similar invariants of the strain tensor:

Note that summation over repeated subscripts is implied

$$I_1 = \varepsilon_{ii} = \Delta$$

$$I_2 = \tilde{\varepsilon}_{ij} \tilde{\varepsilon}_{ij}$$

You can also use $I_2 = \varepsilon_{ij} \varepsilon_{ij}$, this would be just a combination of the invariants shown here

Lagrangian

- Thus, functions L and D for an isotropic linear solid or fluid are obtained by combining all possible quadratic scalar terms satisfying the above requirements:

$$\begin{cases} L = \frac{\rho}{2} \dot{u}_i \dot{u}_i - \left(\frac{\zeta}{2} u_i u_i + \frac{K}{2} \Delta^2 + \mu \tilde{\epsilon}_{ij} \tilde{\epsilon}_{ij} \right), \\ D = \frac{d}{2} \dot{u}_i \dot{u}_i + \left(\frac{\eta_K}{2} \dot{\Delta}^2 + \eta_\mu \dot{\tilde{\epsilon}}_{ij} \dot{\tilde{\epsilon}}_{ij} \right). \end{cases}$$

Material properties d and ζ equal zero for an ordinary material without internal structure.

Thus, there are generally 5 material properties in a structureless rock

- Each term in L and D contains a factor, which is the corresponding **material property**. Meanings of these material properties are established by setting up some mechanical experiment involving this factor (we discuss them later)
- The unit of L is $[\text{energy density}] = [\text{pressure}] = [\text{Pa}]$, and the units for D are $\left[\frac{\text{energy density}}{\text{time}} \right] = \left[\frac{\text{pressure}}{\text{time}} \right]$. Therefore, the units for material properties are:

$$[\rho] = \left[\frac{\text{energy density}}{\text{velocity}^2} \right] = [\text{mass density}]$$

$$[K] = [\mu] = [\text{pressure}]$$

$$[\eta_K] = [\eta_\mu] = [\text{pressure} \cdot \text{time}] = [\text{viscosity}]$$

$$[\zeta] = \left[\frac{\text{pressure}}{\text{m}^2} \right] = \left[\frac{\text{force}}{\text{m}^4} \right]$$

$$[d] = \left[\frac{\text{pressure}}{\text{m}^2 / \text{time}^2} \right] = \left[\frac{\text{viscosity}}{\text{permeability}} \right] = \frac{1}{[\text{mobility}]}$$

Forces, stresses, and equations of motion

- Recall the Euler-Lagrange equations from Lecture 3 for generalized variable $q_i(\mathbf{x}) = u_i(\mathbf{x})$:

$$\frac{\partial}{\partial t} \frac{\partial L}{\partial \dot{q}_i} + \frac{\partial}{\partial x_j} \frac{\partial L}{\partial q_{i,j}} - \frac{\partial L}{\partial q_i} + \frac{\partial D}{\partial \dot{q}_i} - \frac{\partial}{\partial x_j} \frac{\partial D}{\partial \dot{q}_{i,j}} = 0$$

- Considering the case $\zeta = 0$ and $d = 0$, and taking the derivatives, this equation turns out to be:

$$\rho \ddot{u}_i = f_i \quad , \quad \text{where the force is the divergence of a stress tensor } \sigma: \quad f_i = \partial_j \sigma_{ij}$$

- ... and the stress tensor is:

$$\sigma_{ij} = \left(K \Delta \delta_{ij} + 2\mu \tilde{\epsilon}_{ij} \right) + \left(\eta_K \dot{\Delta} \delta_{ij} + 2\eta_\mu \dot{\tilde{\epsilon}}_{ij} \right)$$

Hooke's law -
Elastic stress
proportional to
strain $\tilde{\epsilon}$

Navier-Stokes law -
Viscous stress
proportional to
strain rate $\dot{\tilde{\epsilon}}$

In each pair of parentheses here, the first term is the **bulk elasticity or viscosity**, and the second is the **shear one**

These are “constitutive relations” in mechanics

Medium with internal structure ("General Linear Solid", GLS)

- Internal structure of a rock can be described macroscopically by adding additional variables (fields) to the observable displacement variable $u_i(\mathbf{x}, t)$. There are two ways to add such variables:
 - Using completely different scalar variables, which I combine in another vector field $\boldsymbol{\theta}(\mathbf{x}, t)$
 - Elements of this vector can represent pore volume variations, grain expansions or rotations, temperature variations, etc.
 - This variable $\boldsymbol{\theta}$ will be considered later**
 - Using variables with meanings of displacements of some internal structures
 - Average displacements of pore fluids, relative displacements of groups of grains, etc.
 - These internal-displacement fields can be added to displacement $u_i(\mathbf{x}, t)$, making it a vector in model space, $\mathbf{u}_i(\mathbf{x}, t)$
- With this second type of model extension, L and D functions look the same, but **all material properties become matrix-valued quantities**:

$$\begin{cases} L = \frac{1}{2} \dot{\mathbf{u}}_i^T \boldsymbol{\rho} \dot{\mathbf{u}}_i - \left(\frac{1}{2} \mathbf{u}_i^T \boldsymbol{\zeta} \mathbf{u}_i + \frac{1}{2} \boldsymbol{\Delta}^T \mathbf{K} \boldsymbol{\Delta} + \tilde{\boldsymbol{\epsilon}}_{ij}^T \boldsymbol{\mu} \tilde{\boldsymbol{\epsilon}}_{ij} \right), \\ D = \frac{1}{2} \dot{\mathbf{u}}_i^T \mathbf{d} \dot{\mathbf{u}}_i + \left(\frac{1}{2} \dot{\boldsymbol{\Delta}}^T \boldsymbol{\eta}_K \dot{\boldsymbol{\Delta}} + \dot{\tilde{\boldsymbol{\epsilon}}}_{ij}^T \boldsymbol{\eta}_\mu \dot{\tilde{\boldsymbol{\epsilon}}}_{ij} \right). \end{cases}$$

First rows and columns in matrices \mathbf{d} and $\boldsymbol{\zeta}$ (for the observable displacement) must equal zero to ensure translational invariance (independence of the selection of point
 $u_{1x} = u_{1y} = u_{1z} = 0$)

Other macroscopic variables in a GLS model

- Additional (arbitrary!) scalar variables of macroscopic internal structure can be combined in vector field $\boldsymbol{\theta}(\mathbf{x}, t)$
- Again considering the most general (possible) quadratic terms, functions L and D become

$$\begin{cases} L = L_0 - \frac{1}{2} \boldsymbol{\theta}^T \mathbf{P} \boldsymbol{\theta} + \boldsymbol{\Delta}^T \mathbf{Q} \boldsymbol{\theta}, \\ D = D_0 + \frac{1}{2} \dot{\boldsymbol{\theta}}^T \mathbf{P}' \dot{\boldsymbol{\theta}} - \dot{\boldsymbol{\Delta}}^T \mathbf{Q}' \dot{\boldsymbol{\theta}}. \end{cases}$$

L_0 and D_0 are functions from the original GLS model.

Inertia (term with density) is not considered in this Lagrangian (it is likely negligible)

- Elements of matrices \mathbf{P} , \mathbf{Q} , \mathbf{P}' , and \mathbf{Q}' are the **new material properties**:
 - \mathbf{P} contains **elastic properties** of variables $\boldsymbol{\theta}$
 - \mathbf{P}' contains **viscous properties** of variables $\boldsymbol{\theta}$
 - \mathbf{Q} contains **elastic coupling** of variables $\boldsymbol{\theta}$ with \mathbf{u}
 - \mathbf{Q}' contains **viscous coupling** of variables $\boldsymbol{\theta}$ with \mathbf{u}

As you see, different structures within rock can interact with each other elastically and viscously (and also inertially).

All this is easily seen from the general forms of Lagrangian functions.

Equations of motion

- The Euler-Lagrange equations are also similar to those above, but they become **matrix**
 - They also **contain body forces** from matrices ζ and \mathbf{d} (not only surface stresses as in the viscoelastic model):

$$\rho \ddot{\mathbf{u}}_i = \underbrace{-\zeta \mathbf{u}_i}_{\text{Elastic body force}} - \underbrace{\mathbf{d} \dot{\mathbf{u}}_i}_{\text{Viscous drag}} + \underbrace{\partial_j \sigma_{ij}}_{\text{Elastic and viscous surface forces}}$$

- With variables θ , the equations modify to:

$$\begin{cases} \rho \ddot{\mathbf{u}}_i = -\zeta \mathbf{u}_i - \mathbf{d} \dot{\mathbf{u}}_i + \partial_j \sigma_{ij}, \\ \mathbf{0} = \mathbf{P} \theta + \mathbf{P}' \dot{\theta} - \mathbf{Q}^T \Delta - \mathbf{Q}'^T \dot{\Delta}, \end{cases}$$

This equation with zero mass in the left-hand side means **quasi-static equilibrium** (and kinetic equations) for variables θ .

This equation is similar to the (matrix) Zener's equation:

$$\mathbf{P} \theta + \mathbf{P}' \dot{\theta} = \mathbf{Q}^T \Delta + \mathbf{Q}'^T \dot{\Delta}$$

- ...and stress tensors become:

- Elastic (Hooke's law):

$$\sigma_{ij} = \mathbf{K} \Delta \delta_{ij} + 2\mu \tilde{\epsilon}_{ij} - \mathbf{Q} \theta \delta_{ij}$$

- Viscous (Navier-Stokes law):

$$\sigma_{ij} = \eta_K \dot{\Delta} \delta_{ij} + 2\eta_\mu \dot{\tilde{\epsilon}}_{ij} - \mathbf{Q}' \dot{\theta} \delta_{ij}$$

Examples

- Let us briefly consider three examples from sections 5.3, 7.1 and 7.2 in the text:
 - 1) Static deformation under gravity or thermal forces
 - 2) Steady-state Darcy flow
 - 3) Plane P and S waves
- Some more complex cases are described in the text:
 - Extensional waves in an infinite rod
 - Forced oscillations of a cylinder with thermoelastic effects
 - Layered cylinder

Static equilibrium

- If deformation is independent of time, all time derivatives equal zero, and equations become:

$$\partial_j \boldsymbol{\sigma}_{ij} = \mathbf{0}, \quad \boldsymbol{\sigma}_{ij} = \lambda \Delta \delta_{ij} + 2\mu \boldsymbol{\varepsilon}_{ij}$$

- If material properties are constant in space, then these equations give:

$$(\lambda + \mu) \partial_i \partial_j \mathbf{u}_j + \mu \partial_j \partial_j \mathbf{u}_i = \mathbf{0}$$

This equation needs to be solved for \mathbf{u} with the appropriate boundary conditions

- If there is a uniform gravity g_i applied to the solid (with fluids and other internal variables inside), this equation modifies to

$$(\lambda + \mu) \partial_i \partial_j \mathbf{u}_j + \mu \partial_j \partial_j \mathbf{u}_i = -\rho g_i$$

- If there is a nonuniform temperature \mathbf{T} , the equilibrium is modified by thermoelastic body forces proportional to gradients $\partial_i \mathbf{T}$ in the right-hand side:

$$(\lambda + \mu) \partial_i \partial_j \mathbf{u}_j + \mu \partial_j \partial_j \mathbf{u}_i = -\rho g_i + \mathbf{K} \alpha \partial_i \mathbf{T}$$

Static (Darcy) pore flow

- If some GLS stress (confining, pore pressure, etc.) distribution is created within the rock as in the preceding slide, then the resulting pore flow (or another equivalent of internal motion) is obtained from the part f equation containing matrix **d** (mobility):

$$-\mathbf{d}\dot{\mathbf{u}}_i + \partial_j \boldsymbol{\sigma}_{ij} = \mathbf{0} \quad , \text{ or } \quad \mathbf{d}\dot{\mathbf{u}}_i = \partial_j \boldsymbol{\sigma}_{ij}$$

Boundary conditions are again important for this flow to remain steady or to modify the distribution **u(x)**

Plane P wave

- To obtain a plane P wave traveling in the direction X , we need to consider displacements in the form:

$$u_{Jk} = u_J \delta_{k1}$$

$$\varepsilon_{Jik} = u'_J \delta_{i1} \delta_{k1}$$

$$\Delta_J = \varepsilon_{Jii} = u'_J \quad \text{prime denotes derivative} \quad f' = \frac{\partial f}{\partial x}$$

- Equations of motion become a matrix differential equation for function $\mathbf{u}(x, t)$:

$$\rho \ddot{\mathbf{u}} = -\mathbf{d} \dot{\mathbf{u}} + \mathbf{M} \mathbf{u}'' + \boldsymbol{\eta}_M \dot{\mathbf{u}}''$$

$\mathbf{M} \equiv \mathbf{K} + 4\boldsymbol{\mu}/3$ is the P-wave modulus matrix, $\boldsymbol{\eta}_M \equiv \boldsymbol{\eta}_K + 4\boldsymbol{\eta}_\mu/3$ is the P-wave viscosity matrix

- For a **harmonic** wave, the dependence on x and t consists of harmonic functions:

$$\mathbf{u} = \text{Re} \left[\mathbf{v} \exp(-i\omega t + ikx - \alpha x) \right]$$

ω is the angular frequency,
 k is the wavenumber
 α is the spatial attenuation coefficient

- ...and the final eigenvalue equation for n^{th} wave mode is:

$$\rho^* \mathbf{v}^{(n)} = \gamma^{(n)} \mathbf{M}^* \mathbf{v}^{(n)}$$

$$\gamma \equiv \frac{(k^*)^2}{\omega^2}$$

$k^* \equiv k + i\alpha$ is the complex wavenumber

$\rho^* \equiv \rho + i \frac{\mathbf{d}}{\omega}$ effective density

$\mathbf{M}^* \equiv \mathbf{M} - i\omega \boldsymbol{\eta}_M$ effective modulus

Plane P wave (cont.)

- From the eigenvalue γ obtained for n^{th} mode, the phase velocity of the wave is
- ...and inverse Q -factor (from imaginary part of complex-valued slowness $1/V^*$)

$$V_{\text{phase}} \equiv \frac{\omega}{k} = \frac{1}{\text{Re}\sqrt{\gamma}}$$

$$Q^{-1} = \frac{\text{Im}\sqrt{\gamma}}{2\text{Re}\sqrt{\gamma}}$$

Plane S wave

- For a plane S wave polarized in the direction of axis Y (subscript 2) and traveling in the direction X , the displacement and strain components are:

$$u_{Jk} = u_J \delta_{k2} \quad \varepsilon_{J12} = \varepsilon_{J21} = u'_J / 2$$

$$\Delta_J = 0$$

- Equations of motion become differential equation for function $\mathbf{u}(x,t)$:

$$\rho \ddot{\mathbf{u}} = \mu \mathbf{u}'' + \eta_\mu \dot{\mathbf{u}}''$$

- For harmonic waves, the eigenvalue equation for n^{th} wave mode is:

$$\rho^* \mathbf{v}^{(n)} = \gamma^{(n)} \mu^* \mathbf{v}^{(n)}, \text{ where } \mu^* \equiv \mu - i\omega \eta_\mu \text{ is the effective "viscoelastic" shear modulus}$$

- ...and the equations for V_{phase} and Q^{-1} are the same as in the P-wave case

Extensions of the linear Lagrangian (GLS) model

- Above, we only discussed the case of linear interactions within an isotropic medium without thermal effects. What happens when these restrictions are lifted?

Thermal effects

- Regarding the effects of temperature, the accuracy of the above approximation is difficult to . The equations without temperature are suitable in two limits:
 1. When the deformations are extremely slow, so that the temperature equilibrates by heat flows between parts of the body. In this case, the elastic moduli above are the isothermal (constant-temperature) moduli
 - However, this limit seems impractical in most laboratory and seismic measurements
 2. When the deformations are extremely fast, so that the heat exchange between parts of the body is negligible. In this case, the above moduli are adiabatic moduli. Adiabatic moduli are always larger than isothermal ones.
 - This limit is close to seismic case; however, at low frequencies and for grainy media with small grains, heat flows between grains or pores may cause significant effects on wave propagation and on the behavior of rock samples in the lab
- In reality, temperature T is variable during deformation, and it contributes to bulk pressure

Thermal effects

- The elastic energy in the Lagrangian is replaced with the “free energy” equal $F = E - TS$
 - E is the internal energy (of random particle motions), T is the temperature, S is the entropy
 - F is the energy which can be transformed to mechanical work (product of pressure p and volume change dV)
- As the Lagrangian, the free energy is also constructed by identifying the possible second-order combinations of bulk deformation and temperature variations \mathbf{T} :

$$F(\mathbf{T}) = F_0(T) + \frac{1}{2} \mathbf{u}_i^T \boldsymbol{\zeta} \mathbf{u}_i + \frac{1}{2} \Delta^T \mathbf{K} \Delta + \tilde{\boldsymbol{\varepsilon}}_{ij}^T \boldsymbol{\mu} \tilde{\boldsymbol{\varepsilon}}_{ij} - \Delta^T \mathbf{K} \boldsymbol{\alpha} (\mathbf{T} - \mathbf{T}_0)$$

\mathbf{T}_0 is the equilibrium temperature

- \mathbf{T} is also a model vector, because the different components (pore fluids, grain types) have different temperatures during deformation (this variation of temperature is called the **thermoelastic effect**)
 - $\boldsymbol{\alpha}$ is a diagonal matrix of **volume expansion coefficients** for the different components
- The resulting equation for stress is:

$$\boldsymbol{\sigma}_{ij} = (\mathbf{K} \Delta \delta_{ij} + 2 \boldsymbol{\mu} \tilde{\boldsymbol{\varepsilon}}_{ij}) + (\boldsymbol{\eta}_K \dot{\Delta} \delta_{ij} + 2 \boldsymbol{\eta}_\mu \dot{\tilde{\boldsymbol{\varepsilon}}}_{ij}) - \mathbf{K} \boldsymbol{\alpha} (\mathbf{T} - \mathbf{T}_0) \delta_{ij}$$

- Note that temperature variations create additional bulk stress (**thermoelastic effect**)
 - Additional **kinetic** or **diffusion equations** for temperature should also be added to the mechanical equations

Nonlinear internal friction

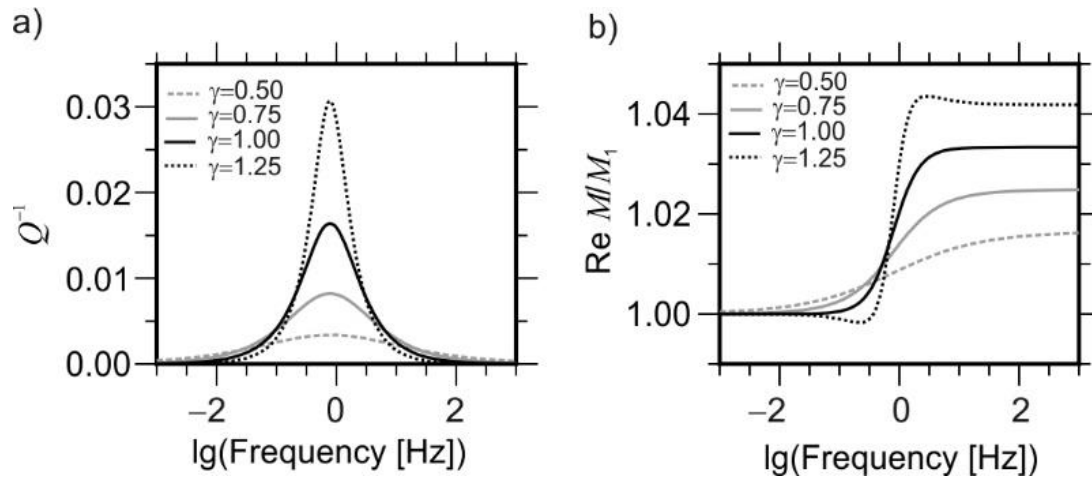
- Nonlinear relations between stresses and displacements and strains are described by non-quadratic forms of the Lagrangian and dissipation function
- The elasticity laws are likely linear (i.e., the Lagrangian quadratic) likely for weak deformations, but dissipation may be nonlinear
 - For example, **dry friction** (Coulomb's law) has $F_{\text{friction}} = \text{const}$, which means dissipation function $D \propto \text{velocity}$ (non-quadratic)
- Thus, we proposed, for example, this dissipation function:

$$D = \frac{1}{\tau_r^2} \left[\frac{1}{2} \left(\tau_r \tilde{\Delta}^{1-\nu_\Delta, \nu_\Delta} \right)^T \boldsymbol{\eta}_K \tilde{\Delta}^{1-\nu_\Delta, \nu_\Delta} \tau_r + \left(\tau_r \tilde{\boldsymbol{\varepsilon}}^{1-\nu_\varepsilon, \nu_\varepsilon} \right)^T \boldsymbol{\eta}_\mu \tilde{\boldsymbol{\varepsilon}}^{1-\nu_\varepsilon, \nu_\varepsilon} \tau_r \right] \quad , \text{ where notation: } \tilde{\Delta}_l^{a,b} \equiv \Delta_l^a \dot{\Delta}_l^b$$

- It increases with $\dot{\Delta}$ slower than with power = 2 (i.e., it is partially “dry”)
 - However, it increases with the total wave amplitude as power = 2, so that the friction acts equally on waves of different amplitudes
 - The nonlinearity is described additional parameters ν (different for bulk and shear)
- This dissipation function (with the usual GLS function L) describes the so-called Cole-Cole rheology (next slide)

Observations of nonlinear internal friction

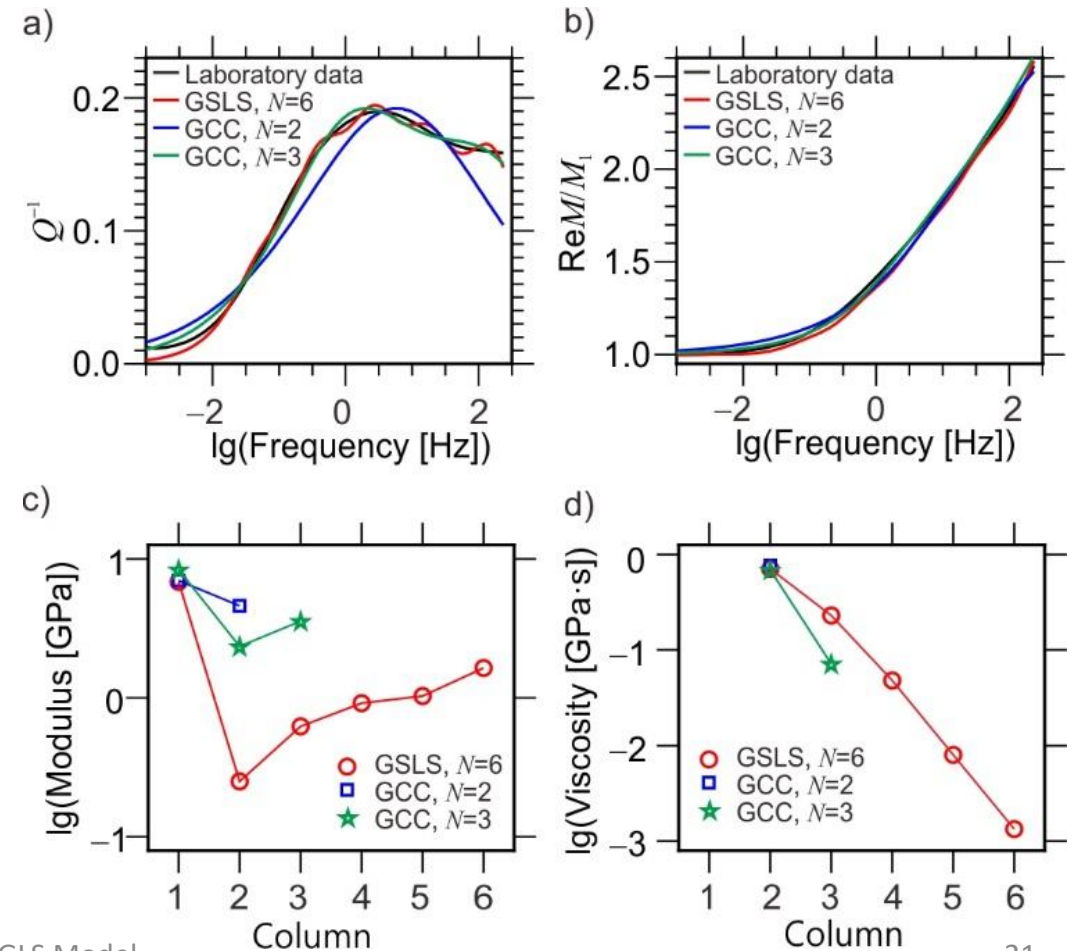
- Cole-Cole spectra predicted by nonlinear SLS (Zener) models with different parameters $\gamma = 2\nu - 1$:



With $\nu = \gamma = 1$, this is the (linear) Zener body response
 Narrower attenuation peaks for $\gamma < 1$,
 broader peaks for $\gamma > 1$

Plots from Deng and Morozov (2016)

- Fitting lab data for bitumen sand (Spencer, 2013)
 - GLS models not only fit data **but obtain values of moduli and viscosity of the sample** (plots c and d)
 - Note that nonlinear models can (sometimes) fit data using smaller values of N



Extensions of the GLS Model

Anisotropic media

- For anisotropic media, there are many more inertial, elastic, and viscous constants in the model. Each term in the Lagrangian and dissipation function becomes a matrix product involving all components of \mathbf{u} or $\boldsymbol{\varepsilon}$ (and not only the rotational invariants)
 - For example, the isotropic elastic energy (case $N = 1$ for simplicity):

$$E_{el} = \frac{\lambda}{2} \Delta^2 + \mu \varepsilon_{ij} \varepsilon_{ij} \equiv \frac{\lambda}{2} \varepsilon_{ii} \varepsilon_{jj} + \mu \varepsilon_{ij} \varepsilon_{ij}$$

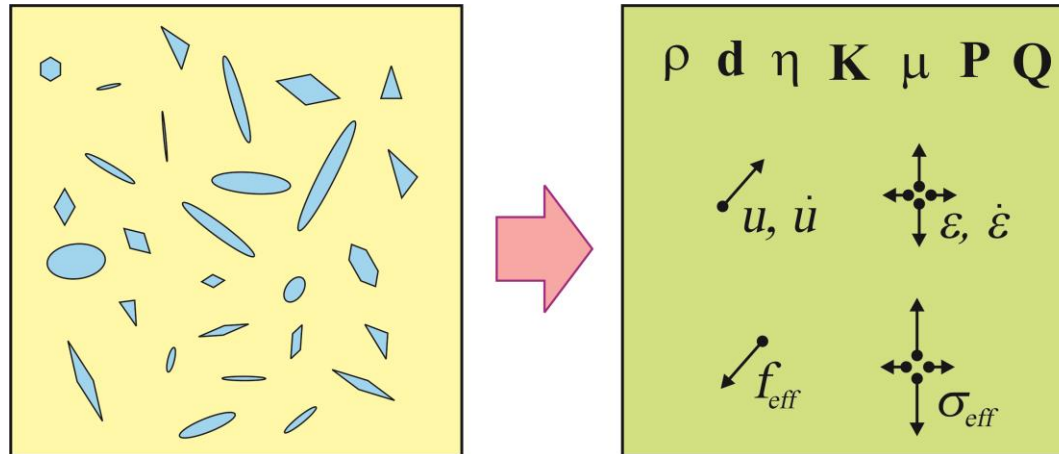
becomes

$$E_{el} = \frac{1}{2} C_{ij|kl} \varepsilon_{ij} \varepsilon_{kl}$$

- The elastic stiffness matrix $C_{ij|kl}$ is a 6 by 6 matrix symmetric with respect to swapping pairs of indices $ij \leftrightarrow kl$
 - Therefore, **there are 21 anisotropic elastic constants**, and similarly 21 constants for viscosity
 - If there are three axes of rotational symmetry (“orthotropic” medium), then there will remain 9 independent elements in matrix $C_{ij|kl}$
- Anisotropic problems are usually easier to consider in coordinate axes of the principal directions of the applied stress

Effective medium

- The concept of “effective medium” refers to the following (typical) situation:
 - Assume we have a rock with known microstructure, such as pores, inclusions, or a digital-rock model
 - This rock is tested in a set of macroscopic mechanical experiments, such as measurement of its drained and undrained moduli, coefficient of thermal expansion, etc.
 - All detail of the microstructure cannot be constrained from the experiment. Therefore, we want to replace the medium with a quasi-homogeneous GLS medium which would account for all of the observations
 - This quasi-homogeneous medium is the “effective medium” described by material-property matrices ρ , \mathbf{d} , η , \mathbf{K} , μ , \mathbf{P} , \mathbf{Q} and similar (here, “ \mathbf{Q} ” is not the Q -factor!):



The state of effective medium is described by average displacement \mathbf{u} and displacement rate $\dot{\mathbf{u}}$, which produce drag friction force \mathbf{f}_{eff} and stress $\boldsymbol{\sigma}_{\text{eff}}$

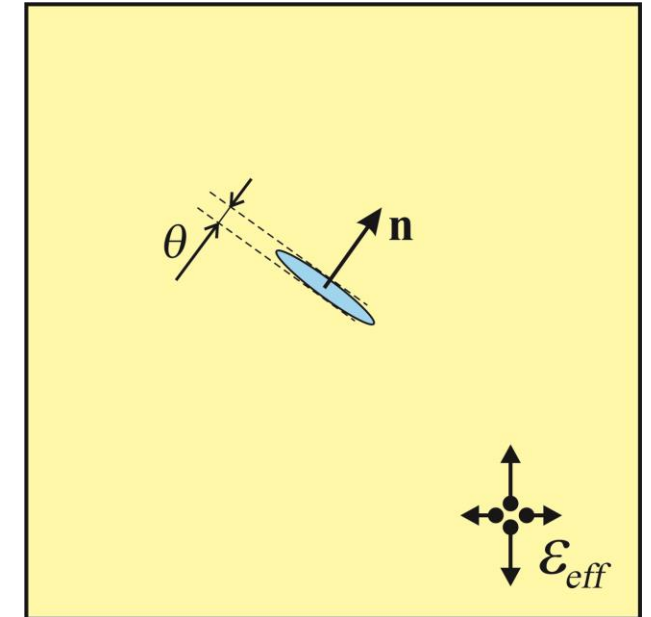
Note that quantities \mathbf{u} , $\boldsymbol{\epsilon}$, \mathbf{f} , and $\boldsymbol{\sigma}$ can be multicomponent (include pore flows, etc.)

- For example, Gassmann’s model is the effective matrix \mathbf{K} for an arbitrary isotropic rock with connected pores under static mechanical testing

Effective medium

- Let us very schematically see how such effective media are obtained for a medium with sparse heterogeneities (typical case)
- First, for a given shape of heterogeneity, its deformation is described by appropriate generalized variables, like θ in this plot:
 - A Lagrangian function $L(\theta, \dot{\theta})$ is constructed for the given shape of the inclusions
- Then, considering an arbitrary deformation of the effective medium, \mathbf{u}_{eff} (and $\boldsymbol{\varepsilon}_{\text{eff}}$), a solution for θ is obtained as a function of \mathbf{u}_{eff} and $\boldsymbol{\varepsilon}_{\text{eff}}$
 - This is done by classical analytical solutions (Eshelby), variational principles (Hashin-Shtrikman), or numerical modeling
 - The change of the Lagrangian due to the inclusion becomes function of the effective strain: $\delta L_{\theta, \mathbf{n}}(\boldsymbol{\varepsilon}_{\text{eff}}, \dot{\boldsymbol{\varepsilon}}_{\text{eff}})$
- The additional Lagrangians due to inclusions are summed over their locations, types, and orientations, giving the total Lagrangian of the effective medium:

$$L(\boldsymbol{\varepsilon}_{\text{eff}}, \dot{\boldsymbol{\varepsilon}}_{\text{eff}}) = L_0(\boldsymbol{\varepsilon}_{\text{eff}}, \dot{\boldsymbol{\varepsilon}}_{\text{eff}}) + \sum \delta L_{\theta, \mathbf{n}}(\boldsymbol{\varepsilon}_{\text{eff}}, \dot{\boldsymbol{\varepsilon}}_{\text{eff}})$$



Typical end-member problem studied in elastostatics – ellipsoidal inclusion in a homogeneous medium (search for “Eshelby problem”, “Eshelby tensor”)